# **Washoe County Development Application**

Your entire application is a public record. If you have a concern about releasing personal information, please contact Planning and Building staff at 775.328.6100.

Project Information	S	Staff Assigned Case No.:	
Project Name:			
Project Description:			
Project Address:			
Project Area (acres or square fe	et):		
Project Location (with point of re	eference to major cross	streets AND area locator):	
Assessor's Parcel No.(s):	Parcel Acreage:	Assessor's Parcel No.(s):	Parcel Acreage:
Indicate any previous Washo Case No.(s).	e County approval	s associated with this applicat	tion:
Applicant Inf	ormation (attach	additional sheets if necess	sary)
Property Owner:		Professional Consultant:	
Name:		Name:	
Address:		Address:	
	Zip:		Zip:
Phone:	Fax:	Phone:	Fax:
Email:		Email:	
Cell:	Other:	Cell:	Other:
Contact Person:		Contact Person:	
Applicant/Developer:		Other Persons to be Contact	ted:
Name:		Name:	
Address:		Address:	
	Zip:		Zip:
Phone:	Fax:	Phone:	Fax:
Email:		Email:	
Cell:	Other:	Cell:	Other:
Contact Person:		Contact Person:	
	For Office	Use Only	
Date Received:	Initial:	Planning Area:	
County Commission District:		Master Plan Designation(s):	
CAB(s):		Regulatory Zoning(s):	

# Tentative Subdivision Map Application Supplemental Information (All required information may be separately attached)

Wh	nat is the location (address or dist	ance and directi	on from ne	earest inter	secti	on)?			
	nat is the subdivision name (podivision)?	roposed name	must not	duplicate	the	name	of	any	existing
De	nsity and lot design:								
a.	Acreage of project site								
b.	Total number of lots								
C.	Dwelling units per acre								
d.	Minimum and maximum area of	proposed lots							
e.	Minimum width of proposed lots								
f.	Average lot size								
Wh	nat utility company or organization	will provide ser	vices to th	e developr	nent:				
a.	Sewer Service								
b.	Electrical Service								
c.	Telephone Service								
d.	LPG or Natural Gas Service								
e.	Solid Waste Disposal Service								
f.	Cable Television Service								
g.	Water Service								
Fo	r common open space subdivisior	ns (Article 408),	please an	swer the fo	llowii	na:			
a.	Acreage of common open space	,	•			Ü			
b.	What development constraints a slope, wetlands, faults, springs,			nt and how	mar	ny acres	s ar	e de	signated
C.	Range of lot sizes (include minir	num and maxim	ium lot size	э):					

d.	Proposed yard setbacks if different from standard:
e.	Justification for setback reduction or increase, if requested:
f.	Identify all proposed non-residential uses:
g.	Improvements proposed for the common open space:
h.	Describe or show on the tentative map any public or private trail systems within common open space of the development:
i.	Describe the connectivity of the proposed trail system with existing trails or open space adjacent to or near the property:
j.	If there are ridgelines on the property, how are they protected from development?
k.	Will fencing be allowed on lot lines or restricted? If so, how?
I.	Identify the party responsible for maintenance of the common open space:
ado http	the project adjacent to public lands or impacted by "Presumed Public Roads" as shown on the opted April 27, 1999 Presumed Public Roads (see Washoe County Engineering website at o://www.washoecounty.us/pubworks/engineering.htm). If so, how is access to those features ovided?
ls t	he parcel within the Truckee Meadows Service Area?
	l Yes □ No

6.

7.

			, coporativo i		as defined by the Req	gioriai i iairi	
	Yes	□ No	If yes, with	nin what city?			
	an arched e the findin		urvey been re	eviewed and	approved by SHPO c	on the prope	rty? If yes, wh
Indic	cate the typ	oe and qu	antity of wate	r rights the ap	oplication has or propo	oses to have	available:
a.	Permit #				acre-feet per year	r	
b.	Certificate	#			acre-feet per year	r	
C.	Surface Cl	laim #			acre-feet per year	r	
d.	Other #				acre-feet per year	r	
			(as filed with		ngineer in the Divisiources):	n of Water	Resources of t
Des	cribe the a	spects of	the tentative :	subdivision th	at contribute to energ	y conservati	on:
enda plea	angered pl	ants and/ species	or animals, ci	ritical breedin	nning and Building as g habitat, migration r ation measures will I	outes or win	ter range? If s
lf pr							
	rided throu			community	be gated? If so, is a	public trail s	system easeme
prov	there any	gh the sul	e policies of the	ne adopted a	be gated? If so, is a rea plan in which the e project comply?		
prov	there any	gh the sul	e policies of the	ne adopted a	rea plan in which the		
Are com	there any there any	applicable f so, whice	e policies of the policies and e area plan me	ne adopted and how does the odifiers in the	rea plan in which the	project is loc	cated that requ
Are com	there any there any	applicable f so, whice	e policies of the policies and e area plan me	ne adopted and how does the odifiers in the	rea plan in which the e project comply?	project is loc	cated that requ

17.		•	rticle 424, Hillside Development? If yes, please address all requirements of a separate set of attachments and maps.
	☐ Yes	□ No	If yes, include a separate set of attachments and maps.
18.			rticle 418, Significant Hydrologic Resources? If yes, please address Special ithin Section 110.418.30 in a separate attachment.
	☐ Yes	□ No	If yes, include separate attachments.
			Grading
(1) bui imp cub yar	Disturbed a ldings and loorted and poic yards of designed to be excepted.	rea exceedi landscaping laced as fil earth to be cavated, wh	ng additional questions if the project anticipates grading that involves: ng twenty-five thousand (25,000) square feet not covered by streets, i; (2) More than one thousand (1,000) cubic yards of earth to be in a special flood hazard area; (3) More than five thousand (5,000) imported and placed as fill; (4) More than one thousand (1,000) cubic ether or not the earth will be exported from the property; or (5) If a e will be established over four and one-half (4.5) feet high:
19.	How many co	ubic yards of	material are you proposing to excavate on site?
20.	anticipated,	where will that measures	of material are you exporting or importing? If exporting of material is e material be sent? If the disposal site is within unincorporated Washoe will be taken for erosion control and revegetation at the site? If none, how rk on-site?
21.			e seen from off-site? If yes, from which directions, and which properties or es will be taken to mitigate their impacts?
22.			ntal/Vertical) of the cut and fill areas proposed to be? What methods will be ntil the revegetation is established?
23.	Are you plan and/or reveg	• .	rms and, if so, how tall is the berm at its highest? How will it be stabilized
24.	with interver	ning terracir	to be required? If so, how high will the walls be, will there be multiple walls ag, and what is the wall construction (i.e. rockery, concrete, timber, by will the visual impacts be mitigated?

Will the grading proposed require removal of any trees? If so, what species, how many, and of what size?
What type of revegetation seed mix are you planning to use and how many pounds per acre do you intend to broadcast? Will you use mulch and, if so, what type?
How are you providing temporary irrigation to the disturbed area?
Have you reviewed the revegetation plan with the Washoe Storey Conservation District? If yes, have you incorporated their suggestions?



Venture Engineering & Consulting Inc. 530 E. Plumb Lane Reno, NV 89502

Phone: (775) 825-9898

# **Project Narrative**

Palomino Farms 34-Lot Subdivision Tentative Map Application

Washoe County, NV

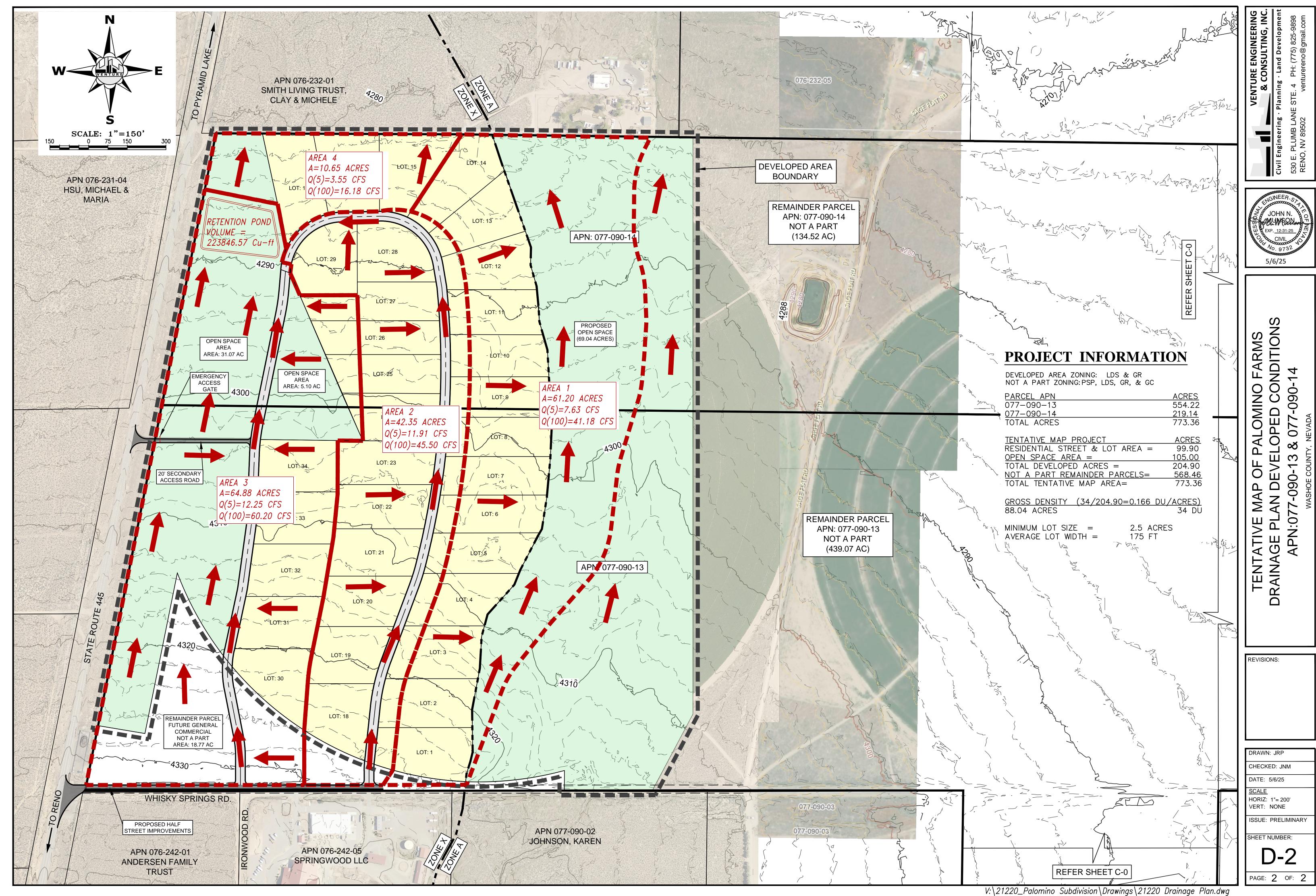
APNs: 007-090-13 and 077-090-14

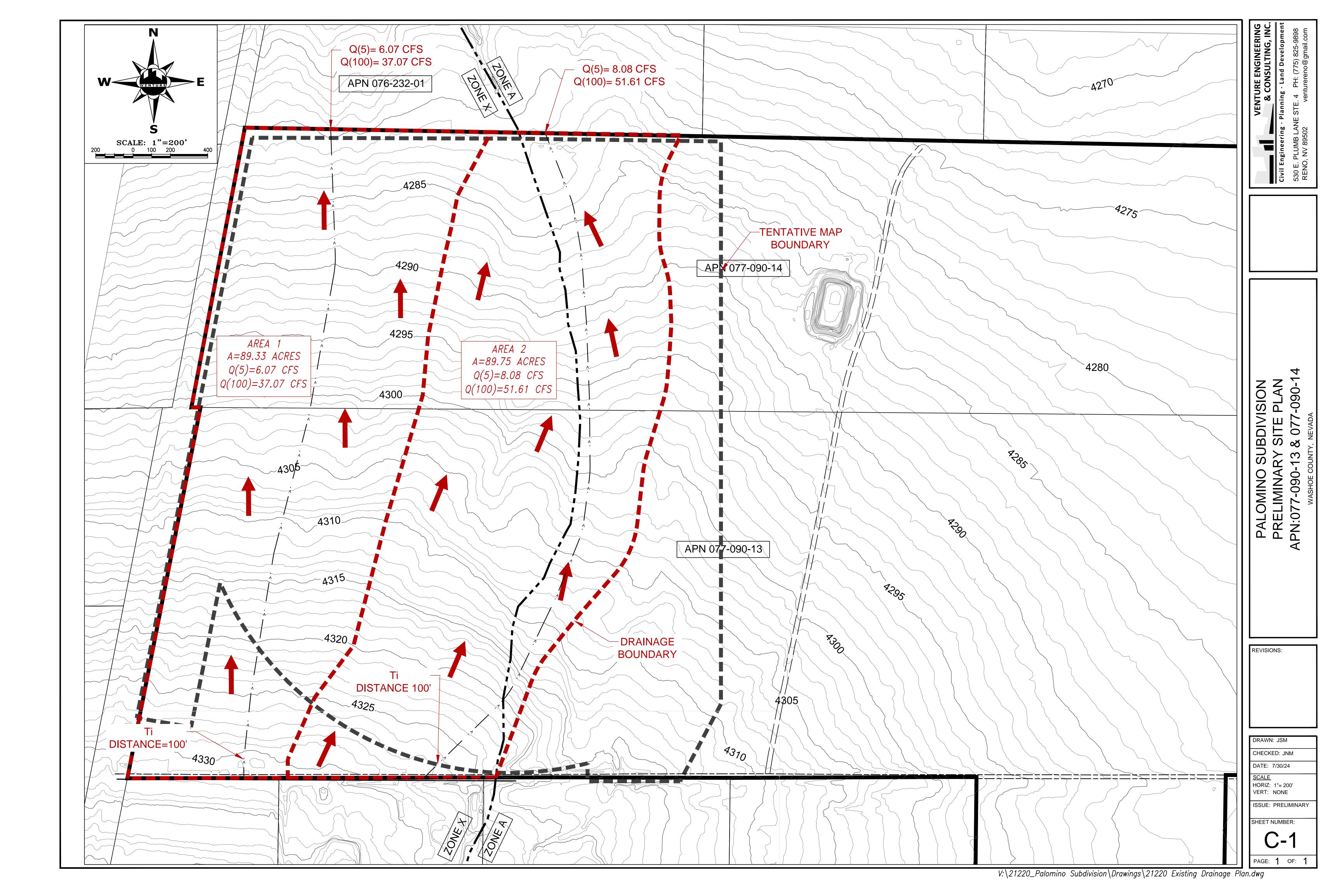
Submitted by: Venture Engineering & Consulting Inc.

Date: May 07, 2025

The Palomino Farms project proposes a 34-lot residential subdivision on a 179.08-acre site located at 0 Whiskey Springs Rd, Washoe County, NV (APNs: 007-090-13 and 077-090-14). The development aims to establish a sustainable rural community in the Palomino Valley by subdividing the property into lots with a minimum size of 2.5 acres. To address flood risk, all residential development has been strategically relocated westward, outside the eastern flood zone identified by the National Flood Hazard Layer. The site, currently vacant land, will preserve environmental integrity by designating a portion of the property as deed-restricted open space, aligning with Washoe County's objectives for balanced rural development.

The project modifies the standard zoning requirement of 5 acres per septic and well to 2.5 acres per septic and well, with an additional 2.5 acres of deed-restricted open space per lot, ensuring a total of 5 acres per septic system. This modification has been approved through a variance granted by the State of Nevada Board of Health, confirming compliance with state regulations for septic system density. Infrastructure improvements, including septic and well systems, adhere to Washoe County Health District standards, and the final map plans align with approved construction and water project plans. The Palomino Farms subdivision reflects a carefully planned approach to rural development, supporting Washoe County's goals for sustainable growth and environmental stewardship.





Serving Reno, Sparks & Washoe County

# District Board of Health Meeting Minutes

Members Thursday, February 27, 2025

Devon Reese, Chair

Clara Andriola, Vice Chair

Paul Anderson

Michael Brown

Dr. Eloy Ituarte Steve Driscoll

Dr. Reka Danko

Washoe County Administration Complex Commission Chambers, Building A 1001 East Ninth Street Reno, NV

1:00 p.m.

# 1. Roll Call and Determination of Quorum.

Chair, Devon Reese, called the meeting to order at 1:00 p.m.

The following members and staff were present:

Members present: Devon Reese (virtual until 1:10 p.m.)

Clara Andriola Paul Anderson Michael D. Brown Dr. Eloy Ituarte Steve Driscoll

Dr. Reka Danko (arrived at 1:05 p.m.)

# Ms. Lawson verified a quorum was present.

# 2. Pledge of Allegiance.

Ms. Clara Andriola led the pledge to the flag.

# 3. Election of District Board of Health Vice Chair for the period 2/17/25-12/31/2026.

Candidates include Clara Andriola, Paul Anderson, Steve Driscoll, Michael Brown, Dr. Eloy Ituarte, and Dr. Reka Danko. (FOR POSSIBLE ACTION)

Chair Reese nominated Clara Andriola for the Vice Chair position. With no opposition to this or other nominations, Paul Anderson seconded the motion, which was approved unanimously.

Chair Reese turned the meeting over to Vice Chair Andriola.

# 4. Approval of Agenda. (FOR POSSIBLE ACTION)

Steve Driscoll motioned to approve the agenda. Michael Brown seconded the motion, and it was approved unanimously.

Vice Chair Andriola asked how the patient payer mix compares year over year in terms of the percentage that has been reported.

Mr. Duplantis reported the mix is shown in the report and is reviewed daily. Before the Affordable Care Act, they saw more uncompensated care and less Medicaid. Afterwards, they were picking up more covered people under Medicaid. In looking at the future, if Medicaid were to change, he expects that there would be a shift between Medicaid and uncompensated care.

Mr. Driscoll asked about who pays for transports out of the area and how that affects the daily fleet in the service area.

Mr. Duplantis noted that REMSA Health does few transports out of the area, but about 40 interfacility transports. One example for out-of-area would be pediatric mental health patients, who get transported to Las Vegas. This takes a unit and its staff out of service for two days. In this situation, they increase staff and equipment to accommodate the shortage.

Vice Chair Andriola thanked Mr. Duplantis on behalf of the Board for all his work on presenting everything and getting the highest level of financial reporting that one entity can achieve.

10. Presentation, discussion, and possible approval of the Regional Emergency Medical Services Authority (REMSA) Health Franchise Compliance Report for the period of 7/1/2023 through 6/30/2024. (FOR POSSIBLE ACTION)

Staff Representative: Andrea Esp

Andrea Esp shared that in 2024, REMSA Health was found compliant in all 17 articles. There was nothing outstanding, with all information provided in the time frame outlined.

Mr. Driscoll moved to approve the Compliance Report. Motion was seconded by Mr. Anderson and approved unanimously.

11. Recommendation to uphold the decision of the Sewage, Wastewater & Sanitation (SWS) Hearing Board to approve Variance Case #H24-0004VARI of the Northern Nevada Public Health Regulations Governing Sewage, Wastewater, and Sanitation, allowing a reduction in minimum lot size for a new subdivision to be served by septic, by holding sufficient additional land open in perpetuity to meet the maximum septic density intended by the regulations, for Palomino Farms LLC, owner of 0 Whiskey Springs Rd/0 Safe Flat Rd, Washoe County, Nevada, Assessor's Parcel Numbers 077-090-013 and 077-090-14. (FOR POSSIBLE ACTION)

Staff Representative: Dave Kelly

Dave Kelly noted that regulations require that any new subdivision being served by septic need a minimum of 5 acres and any proposal that doesn't meet that minimum goes through a variance procedure. This variance was approved by the Advisory Board, requesting a minimum lot size of 2.5 acres to meet the regulatory intended minimum density. They proposed holding open space in two 2.5-acre or more, so the total density meets the criteria. In addition, the new parcels are located outside of the 100-year flood zone, which is an additional benefit to the proposal. The variance allows for slight modifications when going through the planning department processes, as long as the minimum acreage of 2.5 acres is met and the minimum density of 1 septic per 5 acres is not exceeded.

Mr. Driscoll asked if the developer came back in the future, wishing to develop these 2.5-acre sites being held as open space, what would be the process for a variance?

Mr. Kelly noted that this will be recorded as part of the map that it will remain open space unless municipal sewer becomes available.

Mr. Brown motioned to uphold the decision of the SWS Board, with a second by Mr. Driscoll. The motion was approved unanimously.

12. Discussion on the FY26 Budget status, timelines, and next steps.

Staff Representative: Jack Zenteno

Erin Dixon presented a brief overview of the NNPH's budget process and timelines. The Interlocal Agreement requires that the Board of County Commissioners adopt a final budget for NNPH and must be prepared using the same timeframes and format used by other County departments. It also requires that the preliminary budget is presented to the managers of the City of Reno, City of Sparks, and Washoe County for review and comment. The NNPH budget will be presented to the District Board of Health at a special meeting on March 6 at 3:00 p.m. On March 14, NNPH leadership will be meeting with the three jurisdictional partners and the comments from that meeting will be brought back to this Board at the regular March meeting on March 27. The budget will then be included in the County's budget process before the BCC and submitted to the State based on State requirements and timelines. She thanked the members of the Board for their flexibility in being available for the special meeting next week.

13. Recommendation for appointment to the Air Pollution Control Hearing Board as an At-Large Committee Member. Staff recommends: The appointment of Mr. Chaitanya Korra for a three-year term beginning on February 27, 2025, and concluding on February 26, 2028; Applicants include: William Foster McCoy, Ph.D., and Stephen Birdsall. (FOR POSSIBLE ACTION)

Staff Representative: Francisco Vega

Francisco Vega shared his sincere appreciation to all applicants in communicating their interest in joining the Board.

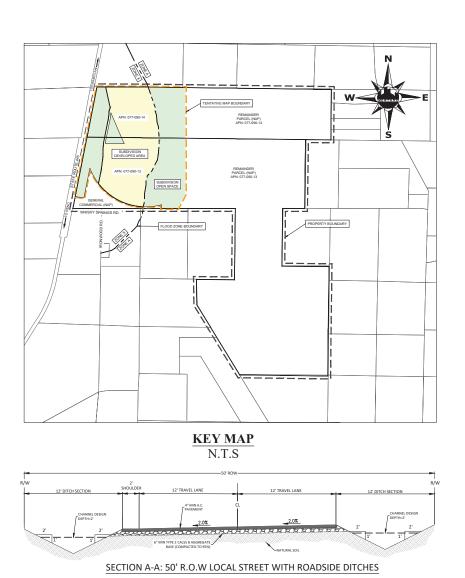
Mr. Anderson moved to accept the appointment as suggested. Mr. Brown seconded the motion, and the item passed unanimously.

14. Review, discussion, and possible adoption of the Business Impact Statement regarding proposed revisions to the District Board of Health Regulations Governing Air Quality Management, Chapter 040 (Prohibited Emissions), Part 040.110 (Asbestos Control Standards), and Part 040.115 (Acknowledgement of Asbestos Assessment) with a finding that the revised regulations do not impose a direct and significant economic burden on a business; and set a public hearing for possible adoption of the proposed revisions to the Regulations for March 27, 2025, at 1:00 p.m. (FOR POSSIBLE ACTION)

Staff Representative: Francisco Vega

Craig Peterson shared the new Air Quality mission statement, which reads the Air Quality Management Division is dedicated to the protection of air quality and the safeguard of public health for all of Washoe County through the development and implementation of effective programs and regulations while supporting economic growth, community partnerships and environmental justice. Revisions to General Source Permitting Regulations, Chapter 030 regarding asbestos were relocated to Chapter 040 under prohibited emissions in September 2024. The sections regarding asbestos have not been reviewed or revised in 25-30 years and do not reflect the intended purpose of the federal regulations. Major changes would include separating the rules into two parts, 040.110 (Asbestos Control Standards) and 40.115 (Acknowledgement of Asbestos

# TENTATIVE SUBDIVISION MAP FOR **PALOMINO FARMS**



SHEET INDEX SHEET NO.

CIVIL ENGINEER

VENTURE ENGINEERING AND CONSULTING, INC.
C/O JOHN MURISON, P.E.
530 E PLIMB LANE, SUITE #4
RENO, IN \$8525-9880
PHONE: 775-825-9880
BMAIL: VENTURERENO/BGBARIL.COM

#### BENCHMARK

THE BASIS OF BEARINGS FOR THE SURVEY IS STATE PLANE NV WEST ZONE. THE BASIS OF ELEVATIONS IS NACDBB.

# FEMA INFORMATION

FIRM: 32031C2675G PROPERTY DESIGNATION: ZONE A,X

#### SITE INFORMATION

TYPICAL LOT SIZE STATISTICS ARE AS FOLLOWS

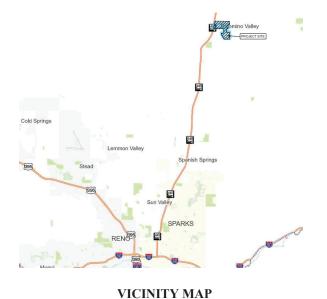
#### PROJECT INFORMATION

MINIMUM LOT SIZE = 2.5 ACRES AVERAGE LOT WIDTH = 175 FT

#### OWNER/DEVELOPER

PALOMINO FARMS LLC 200 MILE CIRCLE DR RENO NV 89511

#### BASIS OF BEARINGS



N.T.S

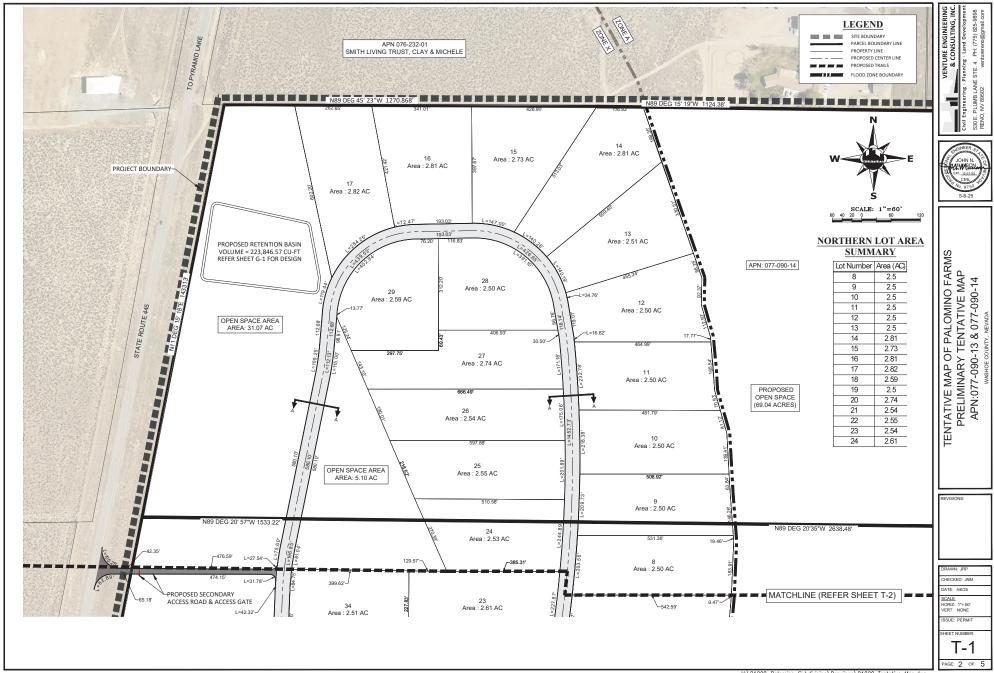
CHECKED: JNM

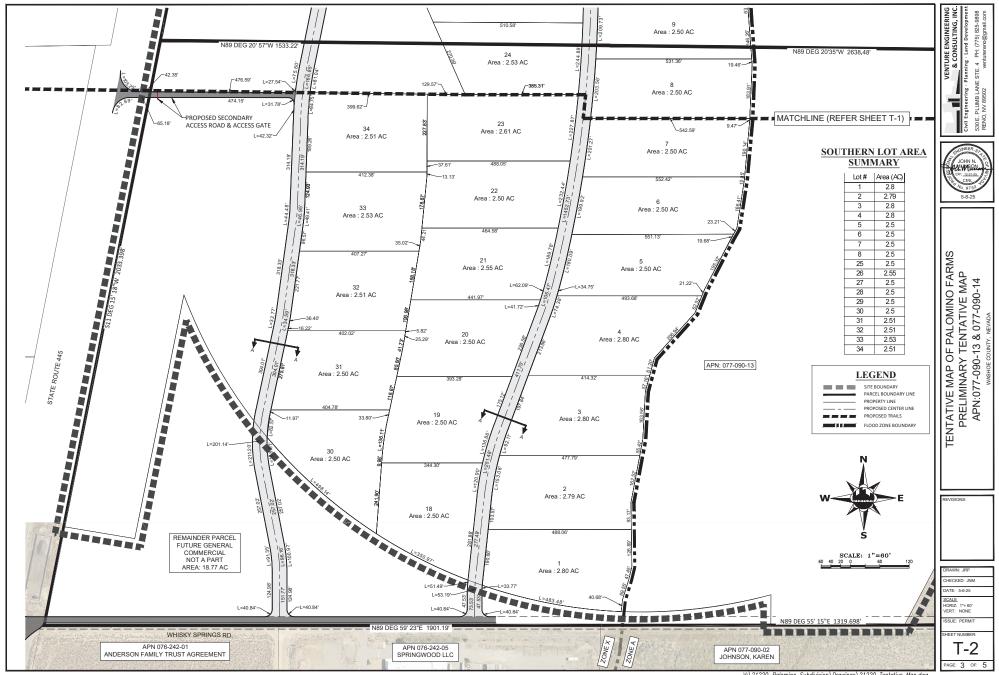
DATE: 5-6-25

TENTATIVE MAP OF PALOMINO FARMS
COVER SHEET
APN:077-090-13 & 077-090-14

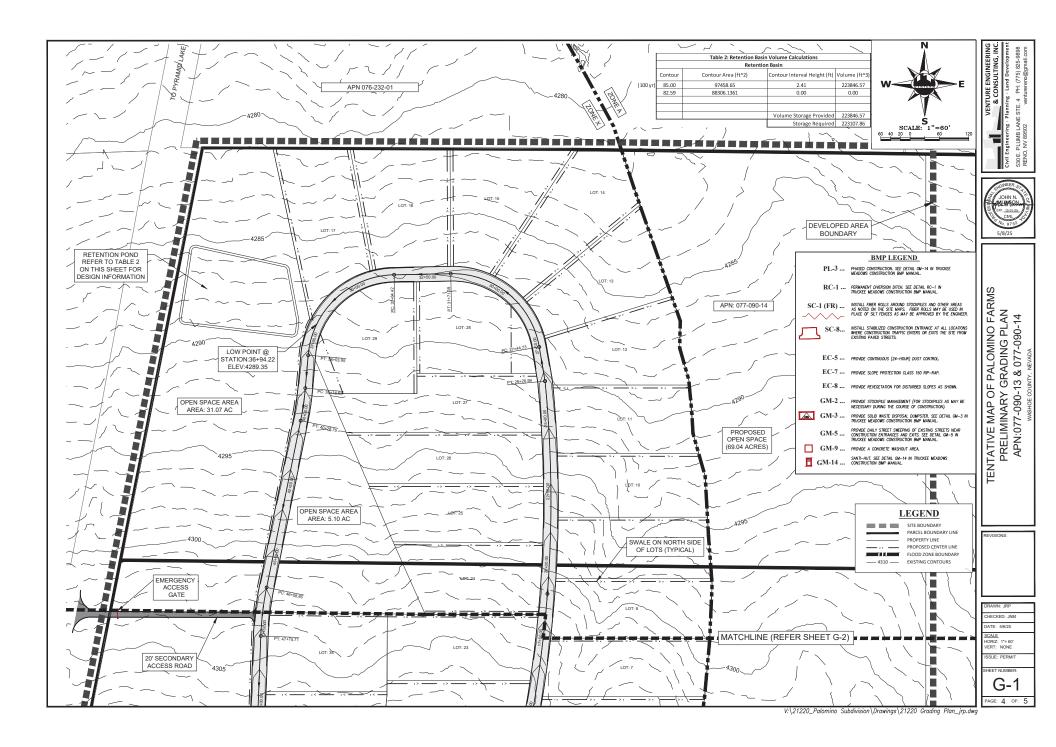
ISSUE: PERMIT

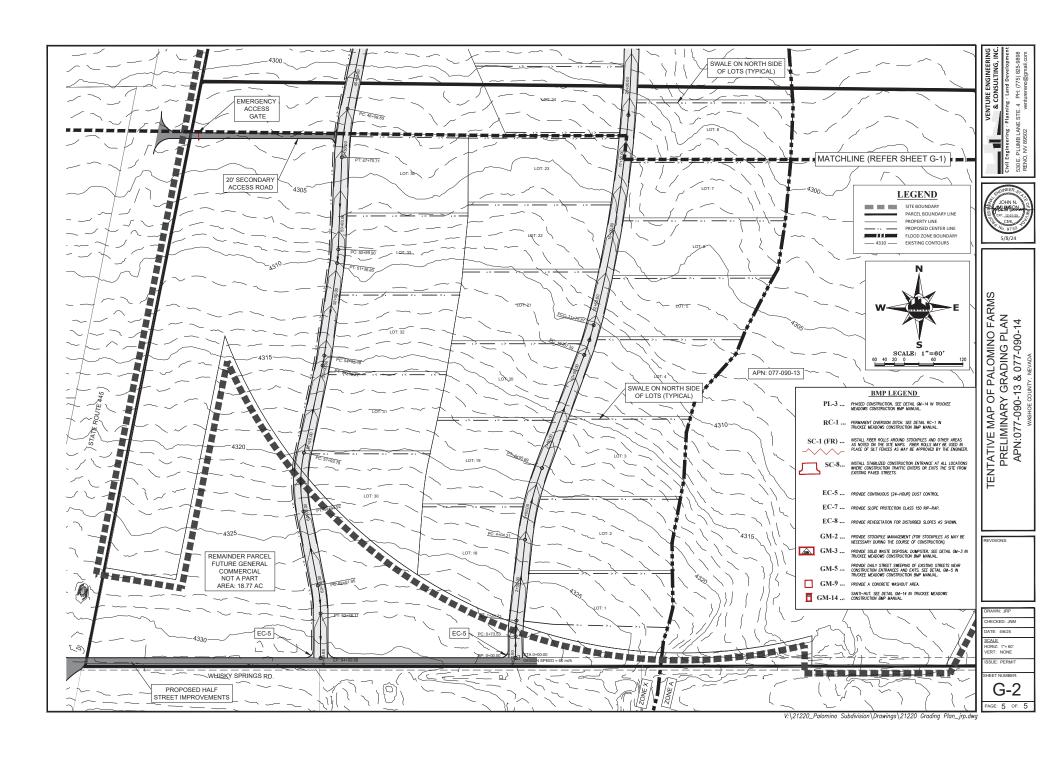
C-0





V:\21220\_Palomino Subdivision\Drawings\21220 Tentative Map.dwg







# PRELIMINARY GEOTECHNICAL INVESTIGATION PROPOSED PALOMINO FARMS SUBDIVISION

Portions of Assessor's Office Parcel Numbers 077-090-13 and -14

**Whiskey Springs Road** 

# **WASHOE COUNTY, NEVADA**

Prepared for:

Brian Murphy Construction and Development, Inc. 695 Mile Circle Drive Reno, Nevada 89511

Attn: Brian Murphy, President

May 7, 2025

Project No. 460.03.24-G



May 7, 2025 Project No. 460.03.24-G

Brian Murphy Construction and Development, Inc. 695 Mile Circle Drive Reno, Nevada 89511

D. BETTS

Attn: Brian Murphy, President

Re: Preliminary Geotechnical Investigation, Proposed Palomino Farms Subdivision,

Portions of Assessor's Office Parcel Numbers 077-090-13 and -14,

Washoe County, Nevada

Dear Mr. Murphy,

Earth Tech is pleased to present results of a preliminary geotechnical investigation our firm conducted for the project. Based on results of our preliminary investigation, experience in the area, and understanding of proposed development, we conclude that, from a geotechnical standpoint, the property is suitable for its intended use. The primary geotechnical concerns are the presence of expansive soil, and the potential presence of clean (little or no binder) soil.

We appreciate having been selected to prepare this preliminary investigation and trust results fulfill your needs. If you, or your design consultants, have questions, please do not hesitate to contact us at (775) 954-6719 or at chris@earthtechnv.com.

Respectfully,

Joshua V. Reyes, E.I.T.

Chris D. Poetts

Chris D. Betts, P.E. President

# TABLE OF CONTENTS

l.	INTRODUCTION1
II.	FIELD EXPLORATION AND LABORATORY TESTS1
III.	SITE AND SOIL CONDITIONS
IV.	GEOLOGIC AND SEISMIC CONSIDERATIONS6
	A. Geology       6         B. Faulting and Seismicity       6         C. Liquefaction       7         D. Slope Stability       7         E. Flooding       7         F. Radon       7
V.	OPINIONS AND DISCUSSIONS7
VI.	REFERENCES
VII.	GLOSSARY OF TEST PROCEDURES
VIII.	DISTRIBUTION
IX.	LIST OF ILLUSTRATIONS

Earth Tech, LLC 681 Edison Way Reno, Nevada 89502 (775) 954-6719

# INTRODUCTION

Earth Tech is pleased to present results of a preliminary geotechnical investigation our firm conducted for the proposed project in the Palomino Valley area. The site is on the north side of Whiskey Springs Road and east side of Pyramid Highway and includes portions of Washoe County Assessor's Office Parcel Numbers 077-090-13 and -14 (Property). Development includes construction of isolated pads for single-family residences and commercial development serviced with on-site water and sewage disposal systems. The structures will have one to two levels, will be wood-framed with joist-supported and/or slab-on-grade floors, and will be supported with shallow conventional spread foundations. Dedicated service streets and private parking areas will be surfaced with asphaltic concrete.

We have not received information concerning foundation loads; however, we anticipate maximum wall loads will be about two to five kip per foot (dead plus live plus snow load) and maximum column loads will be less than 15 kip (dead plus live plus snow load). For frost protection, perimeter foundations will bottom at least 24 inches below lowest adjacent exterior ground surface per code. Structural design will follow criteria outlined in the 2018 *International Residential and Building Codes*.

We anticipate earthwork necessary to attain proposed pad grades and proper site drainage will result in cuts and fills from one to two feet. Neither new slopes nor site earth retaining walls are anticipated. Depth of utility and sewage disposal trenches should be less than ten feet. Existing underground utilities in proposed structural areas will be abandoned or relocated. Earthwork in proposed dedicated areas will be performed in accordance with the 2012 Standard Specifications for Public Works Construction, Revision 8 by the Regional Transportation Commission.

The purpose of our investigation was to provide opinions and discussions concerning geotechnical suitability of the Property for its intended use. Once design parameters, such as building locations, finished floor elevations, foundation types and loads, and grading information have been established, a design-level geotechnical report with detailed information of the subsurface soil conditions and recommendations for design and construction should be prepared.

This report is preliminary and geotechnical in nature and not intended to identify other constraints such as environmental hazards, wetlands determinations, or the potential presence of buried utilities.

### II FIELD EXPLORATION AND LABORATORY TESTS

To attain an overview of underlying soil conditions across the Property, one test boring and a test pit were performed. The test boring was advanced using a Central Mine Equipment (CME) 55 drill rig with 7.125-inch outside diameter hollow-stem augers (HSA), while the test pit was excavated using a Komatsu PC238USLC-11 excavator with a 24-inch bucket. Our subsurface exploration extended to depths of 12 to 15½ feet below ground surface.

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The test boring and pit were positioned in the field using pace and compass and a site plan provided by Venture Engineering and Consulting, Inc. The test boring and pit locations are depicted on Plate 1 with respect to the referenced site plan. Locations are approximate. No greater accuracy is implied.

Our engineer logged the visual descriptions of the earth materials. Representative soil samples were collected from the test boring in an 18-inch split-spoon sampler using a 140-pound safety hammer with a 30-inch drop from a cathead release mechanism. From the test pit, samples were collected using a pick and shovel. To assess permeability of the underlying soil, percolation tests were performed in the test pit. The test boring and pit were loosely backfilled with auger and trench cuttings. Logs of the test boring and pit are presented on Plates 2 and 3. The materials encountered were classified in accordance with the Unified Soil Classification System, which is explained on Plate 4.

The samples were returned to our office to confirm field classifications and to select representative samples for laboratory testing. Results of in-situ dry unit-weights and moisture contents, particle size analyses, Atterberg Limits, and moisture-density relationships are presented on Plates 5 through 9.

## III SITE AND SOIL CONDITIONS

Based on the United States Geological Survey 7.5-Minute topographic map of the Fraser Flat Quadrangle, the site is located in Sections 5 and 6, Township 22 North, Range 21 East, and Sections 31 and 32, Township 23 North, Range 21 East. Elevation is between about 4,200 and 4,300 feet relative to mean sea level.

The portions of the Property proposed for development are undeveloped and vacant. Review of images available on Google Earth reveals these portions have been undeveloped and vacant dating back to 1985, the oldest image available. The development area is bordered by Pyramid Highway to the west, Whiskey Springs Road to the south, pasture to the east and a single-family residence and undeveloped land to the north. In general, the Property is relatively flat and level and matches elevations of adjacent roadways and development.

According to the National Resource Conservation Service *Web Soil Survey* and U.S. Department of Agriculture, Soil Conservation Service (*Soil Survey of Washoe County, Nevada, South Part, Sheet No. 10, dated 1980*), the underlying earth materials consist of Turria loam (#570), Wedertz sandy loam, 2 to 4 percent slopes (#1170), and Pizene sandy loam, 0 to 4 percent slopes (#1240). These units are described as follows:

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Turria loam (#570): This very deep, well-drained soil is on alluvial fans. It formed in alluvium from mixed rock sources. Slopes are 0 to 2 percent. Elevation is 4,500 to 5,000 feet. Typically, the surface layer is light brownish gray loam about 2 inches thick. The subsoil is brown clay loam 10 inches thick. The substratum to a depth of 60 inches is pale brown, stratified sandy loam and silt loam. Permeability is moderately slow. Effective rooting depth is 60 inches or more. Run off is slow, hazard of water erosion is slight, and hazard of soil blowing is slight. This soil is subject to shallow flooding during storms of unusually high intensity. Limitations for shallow excavations are slight. Limitations for dwellings with or without basements are severe due to flooding. Limitations for local roads and streets are moderate due to low load bearing strength, flooding, and susceptibility to frost action. Limitations for septic tank absorption fields are moderate due to flooding and slow percolation rates. Shrink-swell potential is moderate. Frequency of flooding is rare. Depth to high water table is greater than 6.0 feet. Depth to bedrock is greater than 60 inches. Potential frost action is moderate. Risk of corrosion to uncoated steel and concrete is moderate and low. respectively. The main limitations associated with use of this unit for urban development, as described by the soil survey, are low strength, susceptibility to frost heaving, and flooding.

Wedertz sandy loam, 2 to 4 percent slopes (#1170): This very deep, well-drained soil is on alluvial fans. It formed in alluvium derived from mixed rock sources. Elevation is 4,500 to 5,500 feet. Typically, the surface layer is pale brown sandy loam about 6 inches thick. The subsoil is brown sandy clay about 16 inches thick. The upper 12 inches of the substratum is pale brown, weakly cemented sandy loam. The lower part to a depth of 60 inches is pale brown gravelly loamy sand. Depth to weak cementation ranges from 20 to 35 inches. Permeability is moderately slow in the subsoil and upper part of the substratum and rapid in the lower part of the substratum. Available water capacity is moderate. Effective rooting depth is 60 inches or more. Runoff is slow, the hazard of water erosion is slight. The hazard of soil blowing is slight. The soil is subject to flash flooding during storms of unusually high intensity. Limitations for shallow excavations are severe due to caving. Limitations for dwellings with or without basements and for small commercial building are severe due to flooding. Limitations for local roads and streets are moderate due to low strength and frost action. Limitations for septic tank absorption fields are severe due to slow percolation rates and poor filter. The shrink-swell potential is low to moderate. The frequency of flooding is rare. Depth to high water table is greater than 6.0 feet. Depth to bedrock is greater than 60 inches. The potential frost action is moderate. The risk of corrosion to steel and concrete is moderate. Limitations associated with use of this soil for urban development, as defined by the soil survey, are the flooding potential, variable permeability rates, the high clay content, and susceptibility to frost heave.

<u>Pizene sandy loam, 0 to 4 percent slopes (#1240):</u> This very deep, well-drained soil is on alluvial fans and outwash plains. It formed in alluvium derived from mixed rock sources. Elevation is 4,400 to 5,000 feet. Typically, the surface layer is pale brown sandy loam about 6 inches thick. The subsoil is brown sandy clay loam about 15 inches thick. The substratum to a depth of 60 inches is sandy loam. Permeability is moderately slow. Effective rooting depth is 60 inches or more. Runoff is slow, hazard of water erosion is slight, hazard of soil blowing is slight. This soil is slightly affected by salt and alkali in the subsoil. Limitations for shallow excavations are slight. Limitations for dwellings with or without basements are slight. Limitations for local roads and streets are slight. Limitations for septic tank absorption fields are slight. Shrink-swell potential is low to moderate. Frequency of flooding is none. Depth to high water table is greater than 6.0 feet. Depth to bedrock is greater than 60 inches. Potential frost action is low. Risk of corrosion to uncoated steel and concrete is high. The soil survey suggests that this unit is well suited for to use for dwellings and septic tank absorption fields.

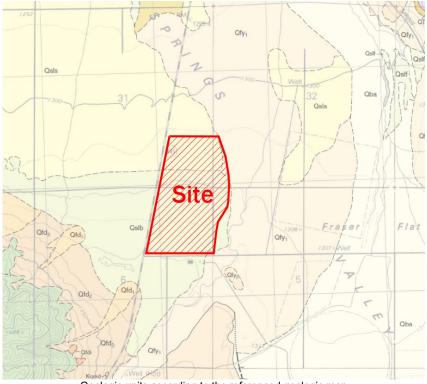


Soils units according to the Web Soil Survey

According to mapping by Larry J. Garside, Stephen B. Castor, Craig M. dePolo, and David A. Davis (*Geologic Map of the Fraser Flat Quadrangle and the West Half of the Moses Rock Quadrangle, Washoe County, Nevada*, Nevada Bureau of Mines and Geology, dated 2003), the material underlying the subject Property consists of Quaternary-age nearshore lacustrine deposits with strandlines (Qslb), and Quaternary-age alluvium covering lacustrine deposits (Qsls). These units are described as follows:

Quaternary-age nearshore lacustrine deposits with strandlines (Qslb): Deposits of silty sand that are largely beach, shoreline, and nearshore deposits from Pleistocene Lake Lahontan. The deposits are moderately sorted with a few cobbles; clasts are subangular to subrounded, with cobbles and gravel that are subrounded to rounded. Deposits are light brown and gray and are non-stratified to moderately stratified.

<u>Quaternary-age alluvium covering lacustrine deposits (Qsls):</u> Light-brown to gray, alluvial, silty sands and sandy silts overlying lacustrine sandy silt deposits. Weakly to moderately stratified. Alluvial deposit thickness varies from 0.1 to about 1 meter. A hummocky surface is common, and pea-gravel lags are locally found at the surface.



Geologic units according to the referenced geologic map

Our subsurface exploration confirms, in general, the referenced soil and geologic mapping with the native soils consisting of light-brown to brown, loose to dense, dry, silty sand (SM), brown, stiff, moist, sandy lean clay (CL), brown, medium dense to very dense, dry, clayey sand with varying amounts of gravel (SC), and light brown, medium dense, dry, silty gravel with sand and occasional cobbles (GM) to the depths explored.

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At the time of our subsurface exploration (April 19 and 24, 2025), no free water or evidence or previous free water was encountered.

Overall, the native soils are in a compact and/or firm density state, exhibit very low (SM and GM soil) to high (CL soil) potential for expansion and low (CL soil) to moderately high (SM and GM soil) Resistance R-Values.

# IV. GEOLOGIC AND SEISMIC CONSIDERATIONS

To evaluate potential geological hazards at the Property, our investigation included a site reconnaissance and review of available literature and maps.

# A. Geology

The property is situated in the Palomino Valley, a structural basin located northeast of Reno and Sparks. This valley is bounded by the Pah Rah Range to the west and the Virginia Mountains to the east, both predominantly composed of Mesozoic granitic and metavolcanic rocks. The valley floor consists of quaternary alluvial deposits derived from the surrounding highlands, forming a relatively flat basin that facilitates surface water accumulation during precipitation events. Drainage within the valley is primarily internal, with limited outflow, leading to the formation of ephemeral playas and shallow ponds in low-lying areas. The region lies within the transitional zone between the Sierra Nevada to the west and the Basin and Range Province to the east, characterized by extensional tectonics and high-angle normal faulting trending in a north-northeast direction. These structural features have influenced the development of the basin's geomorphology and hydrology. Groundwater resources are present within the basin-fill aquifers, although their extent and recharge rates are influenced by the valley's closed drainage system and climatic conditions.

# B. Faulting and Seismicity

According to referenced geologic map, no faults cross the Property. According to *Quaternary Faults in Google Earth* by the USGS, no faults cross the Property. Quaternary-age faults are those which have moved or shifted in the last 1.6 million years. The website indicates that the nearest Holocene- to latest-Pleistocene-age fault is approximately 2.4 miles west of the Property. Faults of this age have moved or shifted in the last 15,000 years.

According to the United States Geologic Survey (USGS) Quaternary Faults website (usgs.maps.arcgis.com), the nearest principal Quaternary-age faults are those associated with the Honey Lake fault zone. Using established empirical relationships (Wells and Coppersmith, 1994) and reported fault parameters, we estimate that an earthquake of magnitude 7.3 is possible along this fault zone.

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# C. Liquefaction

Liquefaction is a loss of soil shear strength associated with loose, saturated, granular deposits subjected to strong earthquake shaking. Liquefaction can result in unacceptable movement of foundations. Generally, liquefaction assessments are reserved for public safety facilities such as fire, police and hospitals or other buildings with high occupancy such as schools. We recommend that the decision to evaluate the potential for liquefaction be considered by the owner or developer during the design-level geotechnical investigation.

# D. Slope Stability

Based on the level nature of the Property and our anticipated depth to groundwater, we do not believe the Property is susceptible to landslides, slumps, or rock falls.

# E. Flooding

The Federal Emergency Management Agency flood map (FEMA-Map 32031C2675G dated March 16, 2009) shows the portions of the Property to be developed in Flood Hazard Zone X unshaded. According to FEMA, Zone X unshaded areas are determined to be outside the 0.2 percent annual chance floodplain.

# F. Radon

Radon, a colorless, odorless, radioactive gas derived from the natural decay of uranium, is found in nearly all rocks and soils. The Environmental Protection Agency (EPA) suggests that remedial action be taken to reduce radon in any structure with average indoor radon of 4.0 picocuries per liter (pCi/L) or more. Based on *Radon in Nevada* (Rigby *et al.*, Nevada Bureau of Mines and Geology, Bulletin 108, 1994), the Property, as well as much of northern Nevada is in, or is in close proximity to, an area where average indoor radon concentrations could exceed 4.0 pCi/L.

# **V OPINIONS AND DISCUSSIONS**

Portions of the underlying soils exhibit a potential for expansion. Expansive soils are subject to substantial volume changes (shrink and swell) with changes in moisture content. Changes in moisture content can occur due to seasonal variations in precipitation, landscape irrigation, broken or leaking water pipes and sewer lines, and/or poor site drainage. These volume changes can cause differential movements (settlement or heave) of foundations, interior slabs-on-grade, exterior flatwork such as walkways, stoops and patios, and pavement sections.

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One method to reduce the potential for movement is to remove (over-excavate) the expansive material to a sufficient depth and replace it with approved compacted fill, thereby reducing the thickness of the expansive layer, providing surcharge, and maintaining moisture at a suitable and near constant level. In conjunction with over-excavation and filling, moisture conditioning of the exposed materials to a slightly over optimum moisture content will be needed during construction. Proper site grading and drainage is necessary for preventing infiltration of water and maintaining the expansive soil at a near-constant moisture content.

Experience has shown that movement of improvements can occur, even if the recommended removal depth is followed, whenever underlying expansive material is allowed to remain. Therefore, the intent of our recommendations is to control this movement without exceeding economic feasibility; however, the owner or developer should weigh the benefits of deeper removal.

Alternatively, to mitigate potential movement, structures can be supported using posttensioned slab-on-ground foundations, which mitigate movement by the rigid nature of the system.

The native soils are relatively clean sand and contain little or no binder such as silt. Consideration should be given to difficulty associated with moisture conditioning and attaining specified compaction percentages associated with clean soils. Consideration should also be given to the potential for instability of excavation sidewalls and the subsequent lateral increase in pit dimensions and trench widths due to widening or overbreak. Stabilization measures such shoring will be necessary to maintain stability and safety.

The soil survey suggests that low strength, susceptibility to frost heaving, variable permeability rates, and flooding can be an additional constraints associated with the use of the underlying soils for urban development. Based on our understanding that foundations will bottom at least 24 inches below lowest exterior ground surface and that structural subbase, aggregate base and proper drainage will be provided within exterior flatwork and pavement areas, we do not believe that low strength and susceptibility to frost heave will adversely impact the Property. Additional percolation testing should be performed during the design-level geotechnical report to assess the potential for variable permeability rates. Based on our review of the referenced FEMA map, the portions of the Property proposed for developed are in an area outside the 0.2 percent annual chance floodplain.

The soil survey also suggests portions of the native soils may exhibit a corrosion potential for uncoated steel or concrete. Assessment of corrosion potential should be performed during the design-level geotechnical report; however, based on our experience in the area, we believe that adequate mitigation can be attained through use of properly prepared and placed, corrosion resistant concrete such as six sack Type II portland cement concrete with 20 percent supplemental cementitious material; by maintaining a minimum 3-inch concrete cover where reinforcing steel or other metal is near native soils and, at the direction of the manufacturer, by using special coating on reinforcing steel and metal.

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In addition to their corrosion potential, consideration should also be given to chemical constituents which may inhibit establishment of landscaping, such as lawns, plants, and other vegetation growth not indigenous to the area. Laboratory testing to determine the agronomic characteristics of the native soils was not part of the scope of our work; however, it should be considered.

Studies regarding the presence of radon gas suggest the Property, as well as much of northern Nevada, is in an area which could exceed the action levels established by the Environmental Protection Agency. Determinations regarding the potential presence of radon gas should be considered prior to site development.

There are no apparent geologic hazards that would place unusual constraints on the project; however, strong ground shaking associated with earthquakes should be expected to occur during the life of the project.

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## **VI REFERENCES**

Federal Emergency Management Agency, U.S. Department of Homeland Security, *FEMA's Flood Map Service Center* (https://msc.fema.gov/portal)

Garside, Larry J., Castor, Stephen B., dePolo, Craig M., Davis, David A. *Geologic Map of the Fraser Flat Quadrangle and the West Half of the Moses Rock Quadrangle, Washoe County, Nevada*. 1:24,000. Reno: Nevada Bureau of Mines & Geology, University of Nevada, Reno, 2003

International Code Council *2018 International Residential and Building Codes*, Whittier: International Code Council, Inc., 2016

Regional Transportation Commission of Washoe County. *Standard Specification for Public Works Construction, Revision 8.* Reno: Regional Transportation Commission of Washoe County, 2012

Rigby, James G., Jonathan G. Price, Lindsay G. Christensen, Daphne D. La Pointe, Alan R. Ramelli, Mario O. Desilets, Ronald H. Hess, and Stanley R. Marshall. *Radon in Nevada*. Reno: Nevada Bureau of Mines & Geology, Bulletin 108, University of Nevada, Reno, 1994

United States Department of Agriculture, Soil Conservation Service. *Soil Survey of Washoe County, South Part, Nevada*. Approved 1980

United States Department of the Interior Geological Survey, *Fraser Flat Quadrangle, Nevada*. 7.5-minute series map (topographic). 1:24,000. Denver: USGS, 2021

United States Department of Agriculture, Soil Conservation Service, Web Soil Survey

Washoe County Health District. Regulations of the Washoe County District Board of Health Governing Sewage, Wastewater, and Sanitation. Amended and Approved on May 23, 2013.

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# VII GLOSSARY OF TEST PROCEDURES

ASTM Test Designation: C 136: Standard Test Methods for Sieve Analysis of Fine and Coarse Aggregates

ASTM Test Designation: D 420: Standard Guide to Site Characterization for Engineering Design and Construction Purposes

ASTM Test Designation: D 1557: Standard Test Methods for Laboratory Compaction Characteristics of Soil Using Modified Effort (56,000 ft-lbf/ft³ (2,700 KN-m/m³))

ASTM Test Designation: D 1586: Standard Test Method for Penetration Test and Split-Barrel Sampling of Soils.

ASTM Test Designation: D 2216: Standard Test Method for Laboratory Determination of Water (Moisture) Content of Soil and Rock by Mass.

ASTM Test Designation: D 2487: Standard Practice for Classification of Soils for Engineering Purposes (Unified Soil Classification System)

ASTM Test Designation: D 2488: Standard Practice for Description and Identification of Soils (Visual-Manual Procedure)

ASTM Test Designation: D 4318: Standard Test Method for Liquid Limit, Plastic Limit, and Plasticity Index of Soils

Section 090 (Percolation Test): Regulations of the Washoe County District Board of Health Governing Sewage, Wastewater, and Sanitation. Amended and Approved on May 23, 2013.

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# **VIII DISTRIBUTION**

One .pdf via e-mail to:

Brian Murphy Construction and Development, Inc. 695 Mile Circle Drive Reno, Nevada 89511 Attn: Brian Murphy, President

One .pdf via e-mail to:

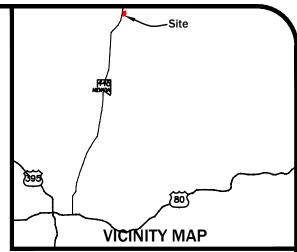
Venture Engineering & Consulting, Inc. 530 E. Plumb Lane Reno, Nevada 89502 Attn: John Munson, Principal Engineer

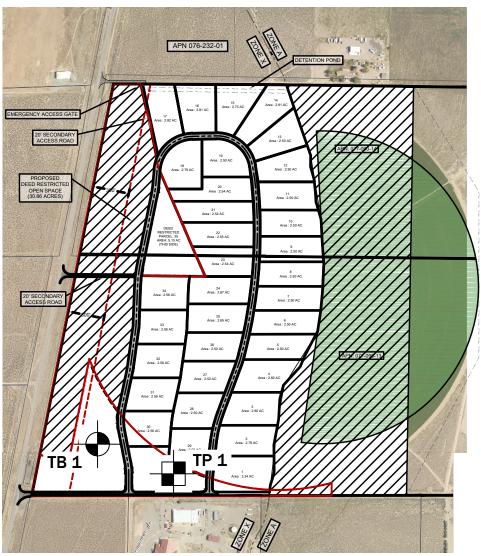
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# IX LIST OF ILLUSTRATIONS

Site and Exploration PlanP	PLATE	1
Log of Test Boring 1P	PLATE	2
Log of Test Pit 1P	PLATE	3
Soil Classification Chart/KeyP	PLATE	4
Particle Size Distribution Report, TB 1, 1.0-3.0'P	PLATE	5
Particle Size Distribution Report, TP 1, 0.5-1.5'P	PLATE	6
Liquid and Plastic Limits Test Report, TB 1, 1.0-3.0'P	PLATE	7
Liquid and Plastic Limits Test Report, TP 1, 0.5-1.5'P	PLATE	8
Compaction Test Report. TB 1. 1.0-3.0'	PLATE	9







Notes: N.T.S

Site plan from Venture Engineering & Consulting, Inc.



Approximate test boring location



Approximate test pit location

Job No. 460.03.24-G

SITE AND EXPLORATION PLAN

Reviewed:

CDB

Earth Tech
Geotechnical and Construction Testing Services
681 Edison Way, Reno, NV 89502

Proposed Palomino Farms Subdivision APNs 077-090-13 and -14 Washoe County, Nevada

Plate 1

Laboratory Tests Plate Numbers and Related Information	Driving Resistance Blows/Ft.	Moisture Content (%)	Dry Density (pcf)	Depth (ft) Sample	Test Boring: TB 1           Equipment         CME 55 w/ 3.75" ID HSA           Elevation         N/A         Date 4/19/2025
* Particle Size Distribution Report (See Plate 5) Liquid and Plastic Limits Test Report (See Plate 7) Compaction Test Report (See Plate 9)	11/6" 28/6"	8.0	114.3 104.9	*1 2 3 4 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	Brown silty sand (SM), loose, dry, with minor roots to three inches deep Becoming medium dense below six inches Brown clayey sand with gravel (SC), very dense, dry, cemented  Brown silty sand (SM), dense, dry
	45			6	Occasional gravel below 8.0 feet
Note: HSA = Hollow Stem Auger GPS: 39.4723139°N	[		<u> </u>		No Free Water Encountered

119.664389°W

Job No. 460.03.24-G

TEST BORING LOG

Reviewed: \_\_CDB

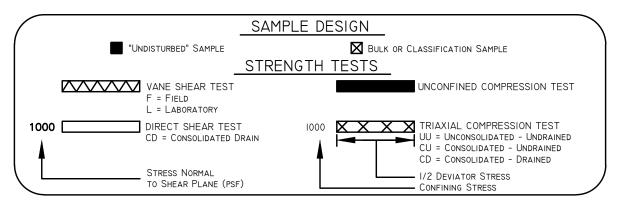
Proposed Palomino Farms Subdivision
APNs 077-090-13 and -14
Washoe County, Nevada

Plate 2

	Φ	(%)	cf)		Te	est Pit: TP 1	
Laboratory Tests Plate Numbers and	Driving Resistance Blows/Ft.	Moisture Content (%)	Dry Density (pcf)	Depth (ft) Sample	Equipment	Komatsu PC238US	SLC
Related Information	Drivi Resi Blow	Mois Cont	Dry Dens	Dept Sam	Elevation N	/A Date 4/2	4/2025
* Particle Size Distribution Report (See Plate 6) Liquid and Plastic Limits Test Report (See Plate 8)  GPS: 39.806150°N 119.660690°W	Drivi Resi Blov	Mois Cont	Dry Pen	1 2 3 4 5 6 7 8 9 10 11 12 12	Elevation N Light-brown silty sand Brown sandy clay (CL) Brown clayey sand (Si Light-brown silty grave (GM), medium dense,	I (SM), loose, dry, with a ), stiff, moist C), medium dense, dry el with sand and occasi dry I (SM), medium dense, d	onal cobbles
Job No. 460.03.24-G			TEST	F PIT LOG		Reviewed:	CDB
Earth Tech Geotechnical and Construction Testing Services 681 Edison Way, Reno, NV 89502	Proposed Palomino Farms Subdivision APNs 077-090-13 and -14 Washoe County, Nevada				e 3		

<u>(                                    </u>	MAJOR DIV	ISIONS	НА	тсн	TYPICAL NAMES
	ODAVELC	CLEAN GRAVELS WITH LITTLE	GW	4	WELL GRADED GRAVELS, GRAVEL-SAND MIXTURES
ILS EVE	GRAVELS  MORE THAN HALF COURSE FRACTION	OR NO FINES	GP	4	POORLY GRADED GRAVELS, GRAVEL-SAND MIXTURES
COARSE GRAINED SOILS MORE THAN HALF IS LARGER THAN #200 SIEVE	IS LARGER THAN No. 4 SIEVE SIZE	GRAVELS WITH	GM	4	SILTY GRAVELS, POORLY GRADED GRAVEL-SAND SILT MIXTURES
AINEI		OVER 12% FINES	GC		CLAYEY GRAVELS, POORLY GRADED GRAVEL- SAND-CLAY MIXTURES
GR/	CANDO	CLEAN SANDS WITH LITTLE	sw		WELL GRADED SANDS, GRAVELLY SANDS
ARSE RE THAN	SANDS  MORE THAN HALF COURSE FRACTION	OR NO FINES	SP		POORLY GRADED SANDS, GRAVELLY SANDS
CO/	IS SMALLER THAN No. 4 SIEVE SIZE	SANDS WITH	SM		SILTY SANDS, POORLY GRADED SAND-SILT MIXTURES
		OVER 12% FINES	sc		CLAYEY SANDS, POORLY GRADED SAND-CLAY MIXTURES
S			ML		INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY
FINE GRAINED SOILS WORE THAN HALF IS SMALLER THAN #200 SIEVE	SILTS AN	ND CLAYS LESS THAN 50	CL		INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS SILTY CLAYS, LEAN CLAYS
VED			OL		INORGANIC CLAYS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
RAII			мн		INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SANDY OR SILTY SOILS, ELASTIC SILTS
FINE G		ND CLAYS REATER THAN 50	СН		INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS
HORE			ОН		ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS
$\bigcup$	HIGHLY ORGAN	NIC SOILS	Рт	<b>***</b>	PEAT AND OTHER HIGHLY ORGANIC SOILS

## UNIFIED SOIL CLASSIFICATION SYSTEM



## KEY TO TEST DATA

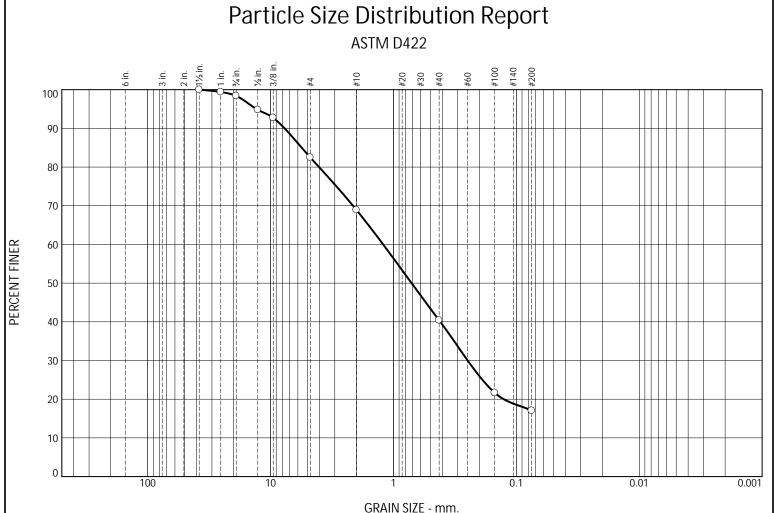
Job No. 460.03.24-G

SOIL CLASSIFICATION CHART/KEY

Reviewed: CDB

Proposed Palomino Farms Subdivision
APNs 077-090-13 and -14
Washoe County, Nevada

Plate 4



				0.0 0.22					
% +3"	% Gi	ravel		% Sand		% Fines			
76 +3	Coarse Fine		Coarse	Medium	Fine	Silt	Clay		
0.0	1.6 15.9		13.6	28.5	23.4	17.0			

	Test Res	sults (ASTM D42	22)	
Sieve Size or Diam. (mm.)	Finer (%)	Spec.* (%)	Out of Spec. (%)	Pct. of Fines
1.5" 1.0" .75" .50" .375" #4 #10 #40 #100 #200	100.0 99.4 98.4 94.8 92.8 82.5 68.9 40.4 21.7 17.0			96.3 94.3 83.8 70.0 41.1 22.0 17.3

PL= 16	Atterberg Limits LL= 24	PI= 8
D <sub>90</sub> = 7.6838 D <sub>50</sub> = 0.7117 D <sub>10</sub> =	Coefficients D85= 5.5763 D30= 0.2490 Cu=	D <sub>60</sub> = 1.2132 D <sub>15</sub> = C <sub>C</sub> =
USCS= SC	Classification AASHTO=	A-2-4(0)
	Test Remarks	

Sample Date:

04-21-2025

**Material Description** 

Brown clayey sand with gravel (SC)

(no specification provided)

Reno, NV, 89502

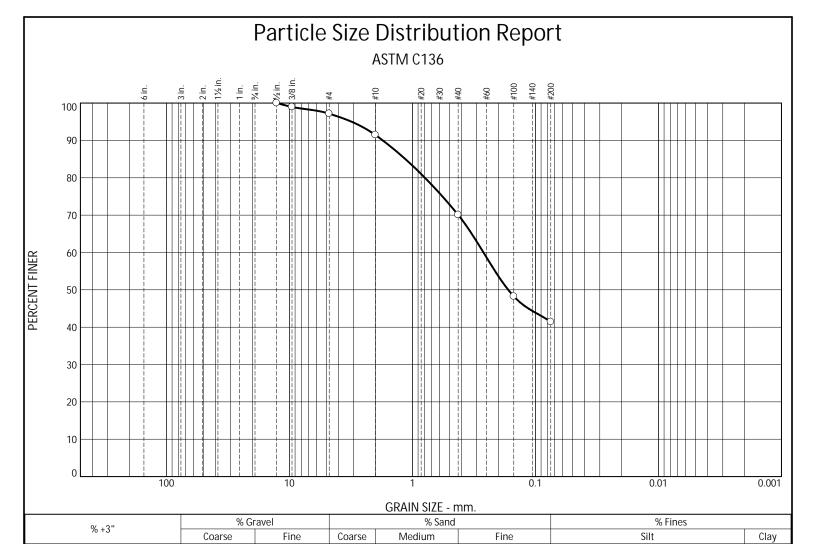
Source of Sample: Test Boring #1 Sample Number: 25-086

Depth: 1.0-3.0'

Earth Tech Client: Brian Murphy Construction and Development

681 Edison Way

Project No: 460.03.24-G Plate 5



21.4

	Test Re	sults (ASTM C13	36)	
Sieve Size or Diam. (mm.)	Finer (%)	Spec.* (%)	Out of Spec. (%)	Pct. of Fines
1/2" 3/8" #4 #10 #40 #100 #200	100.0 99.0 97.2 91.5 70.1 48.3 41.4			

0.0

2.8

5.7

 $\frac{\text{Material Description}}{\text{Brown clayey sand (SC)}}$   $\text{PL= 16} \qquad \frac{\text{Atterberg Limits}}{\text{LL= 47}} \qquad \text{Pl= 31}$   $\frac{\text{Coefficients}}{\text{D}_{50}=\ 0.1665} \qquad \frac{\text{D}_{85}=\ 1.1415}{\text{D}_{30}=\ C_{\text{U}}=\ C_{\text{C}}=}$   $\frac{\text{Classification}}{\text{C}_{\text{U}}=\ C_{\text{C}}=}$   $\text{USCS= SC} \qquad \frac{\text{Classification}}{\text{AASHTO}=\ A-7-6(7)}$   $\frac{\text{Test Remarks}}{\text{Test Remarks}}$ 

Sample Date:

4/24/2025

41.4

(no specification provided)

Source of Sample: Test Pit #1 Sample Number: 25-096

0.0

Depth: 0.5-1.5'

Earth Tech
681 Edison Way

Client: Brian
Project: Pal

Reno, NV, 89502

Client: Brian Murphy Construction and Development

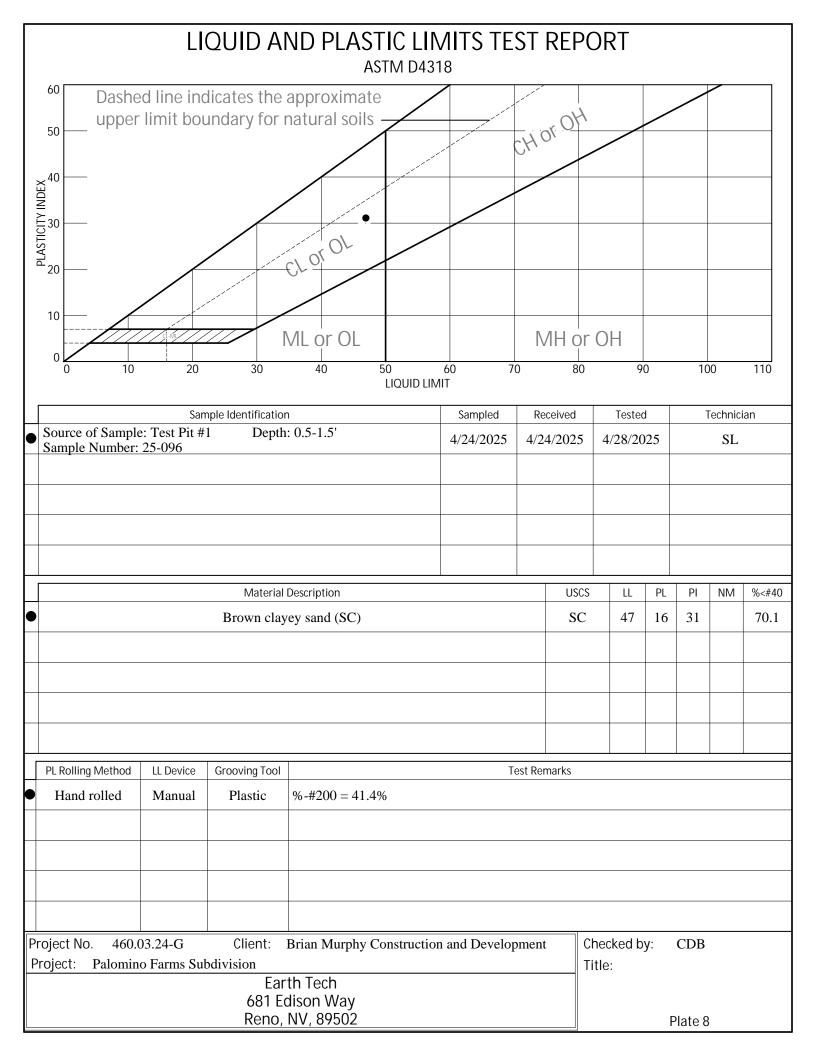
Project: Palomino Farms Subdivision

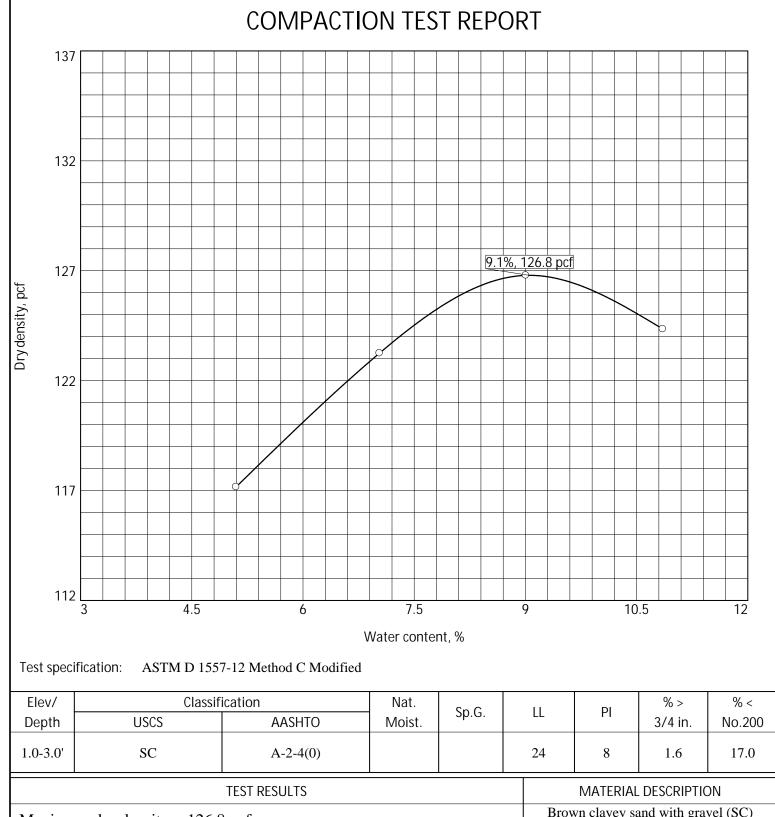
Project No: 460.03.24-G Plate 6

28.7

Tested By: BL Checked By: CDB

		LI	QUID AI	VD PLAS	ΓIC LIN STM D431		ST RE	POI	RT				
60 50				approximate natural soils			CH or O	H					
40 BLASTICITY INDEX 50 10				CL or OL									
0		CL-ML/		ML or OL			MH						
	0 10	20	30	40	50 LIQUID LIM	60 7 IT	0	80	9	0	10	)()	110
• Sou San	arce of Sample	e: Test Bori	nple Identification ng #1 D	epth: 1.0-3.0'		Sampled 04-21-2025	Received	t	Tested	d	-	Technici SL	an
•		Bro		Description  nd with gravel (S	SC)			scs SC	LL 24	PL 16	PI 8	NM	%<#40 40.4
PL F	Rolling Method	LL Device	Grooving Tool				est Remarks						
	land rolled	Manual	Plastic	Percent passing	g sieve #200								
Project Project		03.24-G o Farms Sul	bdivision Ear 681 Ed	Brian Murphy C th Tech dison Way NV, 89502	Construction	and Develop	oment	Che Title	cked b		CDB	,	





TEST RESULTS	MATERIAL DESCRIPTION
Maximum dry density = 126.8 pcf	Brown clayey sand with gravel (SC)
Optimum moisture = 9.1 %	
Project No. 460.03.24-G Client: Brian Murphy Construction and Development	Remarks:
Project: Palomino Farms Subdivision	
Date: 04-21-2025	
Source of Sample: Test Boring #1 Sample Number: 25-086	
Earth Tech	
681 Edison Way	
Reno, NV, 89502	Plate 9

## PRELIMINARY HYDROLOGY REPORT

**FOR** 

## PALOMINO FARMS LLC

0 WHISKEY SPRINGS RD Reno, NV 89511

#### PREPARED FOR:

PALOMINO FARMS LLC 200 MILE CIRCLE DR. Reno, NV 89511

#### PREPARED BY:



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May 6th, 2025

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Digitally signed by John Munson Date: 2025.05.07 Munson Date: 2025.05.0. 14:41:44 - 07'00'



#### 1. Introduction

This hydrology report supports the development application for the Palomino Farms 34-lot subdivision located at 0 Whiskey Springs Rd, Washoe County, NV (APNs: 007-090-13 and 077-090-14). The project involves subdividing 179.08 acres into 34 residential lots, each with a minimum size of 2.5 acres, to relocate development out of the eastern flood zone while maintaining environmental balance through deed-restricted open space. This report evaluates stormwater runoff under existing and proposed developed conditions, ensuring compliance with Washoe County stormwater management standards.

## 2. Site Description

- Location: 0 Whiskey Springs Rd, Washoe County, NV (APNs: 007-090-13 and 077-090-14).
- Total Drainage Area Analyzed: 179.08 acres.
- Existing Conditions: The site is currently vacant land, with drainage flowing to the northeast. The existing drainage pattern is divided into two basin areas, as shown in the attached Existing Conditions Map.
- Proposed Development: The project subdivides the area into 34 lots, each a minimum of 2.5 acres, to
  shift development westward out of the flood zone to the east. The remaining area will be deedrestricted as open space to preserve environmental integrity. The proposed drainage is divided into four
  basin areas, as depicted in the attached Developed Conditions Map.

## 3. Hydrologic Analysis

The hydrologic analysis was conducted using the Rational Method, a standard approach for urban and rural watersheds, as outlined in the Washoe County Development Code and Public Works Design Manual. The Rational Method calculates peak runoff using the formula:

 $Q = C \times I \times A$ 

#### Where:

- (Q) = Peak runoff rate (cubic feet per second, cfs)
- (C) = Runoff coefficient (dimensionless)
- (I) = Rainfall intensity (inches per hour, in/hr)
- (A) = Drainage area (acres)

### 3.1 Design Criteria

- Design Storms: 5-year and 100-year storm events, per Washoe County standards.
- Time of Concentration (Tc): Calculated for both existing and developed conditions using the same methodology. The Tc is determined by summing the initial overland flow time for the first 100 feet and the travel time for the remaining distance. For existing conditions, these calculations are detailed in Table A: Existing Conditions Time of Concentration Calculations. The same method is applied for the developed conditions, with calculations provided in Table B: Developed Conditions Time of Concentration Calculations.
- Rainfall Intensity (I): Interpolated using NOAA Atlas 14 intensity-duration-frequency (IDF) curves, based
  on the total calculated Tc for each basin. The specific (I) values are highlighted in green in Tables A and
  B and are used in Table 1 with composite (C) values and basin areas to compute (Q).
- Runoff Coefficients (( C )): Composite ( C ) values for 5-year and 100-year events were obtained from Table 202 of the Washoe County Public Works Design Manual. Specific ( C ) values for each basin are provided in Table 1.

## 3.2 Existing Conditions

The existing 179.08-acre site drains to the northeast and is divided into two basin areas (see Existing Conditions Map). The time of concentration (Tc) for each basin was calculated by adding the initial overland flow time for the first 100 feet to the travel time for the remaining distance, as detailed in Table A: Existing Conditions Time of Concentration Calculations. Using the interpolated (I) values (highlighted in green in Table A), composite (C) values, and basin areas, the peak runoff (Q) for each basin was computed. The total existing flows are:

- Q (5) = 14.15 cfs
- Q (100) = 88.68 cfs

These flows are summarized in Table 1: Existing Versus Developed Conditions.

#### 3.3 Proposed Developed Conditions

The proposed development divides the 179.08-acre area into four drainage basins (see Developed Conditions Map). Each lot is a minimum of 2.5 acres, allowing the developed area to be shifted west, out of the eastern flood zone, with the remaining land deed-restricted as open space. The drainage areas are as follows:

- Area 1: Drains east, consistent with existing conditions.
- Area 2 and Area 3: Flow north and west into a large retention basin designed to hold the 100-year storm event, retaining the entire increase in runoff (see Table 1). Roadside ditches are provided to facilitate flow.
- Area 4: A small area that flows north, as it does currently.

The time of concentration (Tc) for each of the four basins was calculated using the same methodology as the existing conditions: initial overland flow time for the first 100 feet plus travel time for the remaining distance, as detailed in Table B: Developed Conditions Time of Concentration Calculations. The corresponding (I) values were interpolated using NOAA Atlas 14 data (highlighted in green in Table B). These (I) values, along with composite (C) values and basin areas, were used to compute the peak runoff (Q) for each basin in Table 1: Existing Versus Developed Conditions. Total flows for Areas 1–4 are:

- Q (5) = 35.34 cfs
- Q (100) = 163.06 cfs

The increase in flow from existing to proposed conditions is:

- Q (5) increase = 35.34 14.15 = 21.19 cfs
- Q (100) increase = 163.06 88.68 = 74.38 cfs

#### 3.4 Stormwater Mitigation

To address the increase in runoff (quantified in Table 1: Q (5) increase = 21.19 cfs & Q (100) increase = 74.38 cfs, a large retention basin is proposed for Areas 2 and 3. The required retention volume for the 100-year storm event, as shown at the bottom of Table 1: Existing Versus Developed Conditions, is 223,107.86 cubic feet. The retention basin is designed to provide a storage volume of 223,846.57 cubic feet, as detailed in Table 2: Detention Design Information, which exceeds the required volume by 738.71 cubic feet, ensuring sufficient capacity to retain the entire increase in runoff for the 100-year storm event with a margin of safety. Roadside ditches are provided to direct flows from Areas 2 and 3 into the retention basin, while Area 1 continues to drain east, and Area 4 flows north, both maintaining existing drainage patterns.

## 4. Compliance with Approved Plans

The stormwater management design in the final map plans aligns with:

• Construction Permit Plans: Submitted to Washoe County on May 8, 2025], including grading and drainage specifications.

No deviations exist between the final map plans and the submitted construction plans, ensuring compliance with Washoe County and regional requirements.

#### 5. Conclusion

The proposed Palomino Farms 34-lot subdivision at 0 Whiskey Springs Rd will not result in adverse downstream flooding or water quality impacts. The stormwater management plan, incorporating a large retention basin for Areas 2 and 3 with a provided storage volume of 223,846.57 cubic feet (exceeding the required 223,107.86 cubic feet for the 100-year storm event), effectively mitigates the increase in runoff (Q (5) increase = 21.19 cfs & Q(100) increase = 74.38 cfs). The final map plans are consistent with the submitted construction plans, as verified in Section 4. All design elements comply with Washoe County standards.

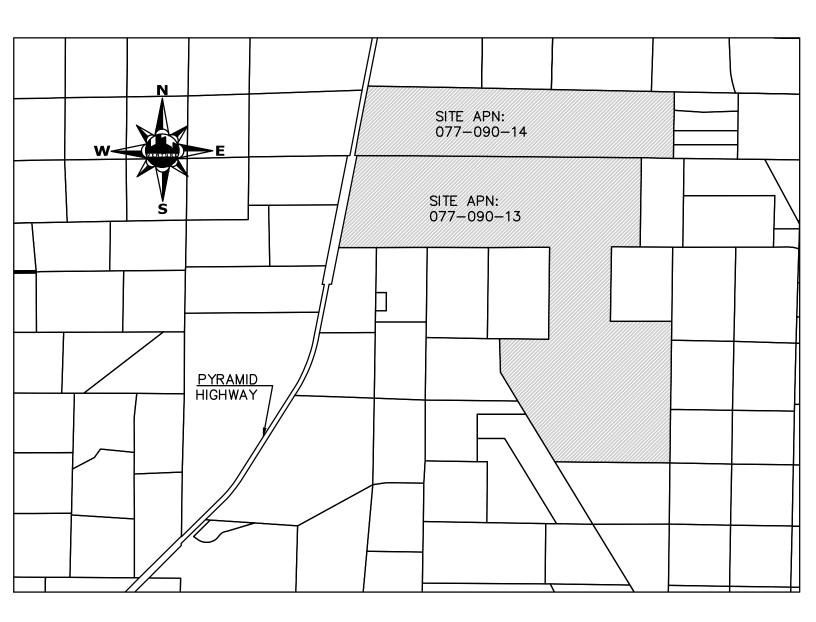
#### Attachments:

- Vicinity Map
- Table A: Existing Conditions Time of Concentration Calculations
- Table B: Developed Conditions Time of Concentration Calculations
- Table 1: Existing Versus Developed Conditions
- Table 2: Detention Design Information
- Existing Conditions Map
- Developed Conditions Map
- Runoff C Values
- NOAA Atlas 14 Table with Rainfall Intensity Data
- Flood Map

#### References:

- Washoe County Public Works Design Manual, Table 202 (Runoff Coefficients).
- NOAA Atlas 14 (Rainfall Intensity Data for Washoe County, NV).

## **APPENDIX**



VICINITY MAP NTS

## Table A - Existing Conditions - Rational Method Tc=Ti+Tt for Intensity Calculations

(Modified Truckee Meadows Reagional Drainage Manual Table 703)



	EXISTING CONDITIONS HYDROLOG													
SUB-BASIN DATA INITIAL/OVERLAN				TIME (Ti)		Overland Flow	Travel Time (Tt)		Tc (Ti+Tt)					
Basin Area	Basin Area R (C value) Length (ft) Slope				Length (ft)	Slope	Velocity (fps)	Tt (min)	Tc (min)					
1	0.2	100.00	0.811	17.37					17.37					
1					959.90	1.687	0.9	17.77586852	17.78					
1					2701.01	0.696	0.57	78.97675439	78.98					
				SUM TIME	Time 1 (Min)	NOAA I Value	Time 2 (Min)	NOAA I Value	Intensity (in/hour)					
	I	ntensity Inter	polation	114.12	60	0.529	120	0.325	0.34					

	EXISTING CONDITIONS HYDROLOGY (5 YEAR)														
SUB-BA	ASIN DATA	INITIAL/O	VERLAND	TIME (Ti)		Overland Flow	Travel Time (Tt)		Tc (Ti+Tt)						
Basin Area	R (C Value)	Length (ft)	Slope	Ti (min)	Length (ft)	Slope	Velocity (fps)	Tt (min)	Tc (min)						
2	0.2 100.00 1.665		13.67					13.67							
2					1112.42	1.635	0.87	21.31073755	21.31						
2					2311.79	1.414	0.82	46.98764024	46.99						
				SUM TIME	Time 1 (Min)	NOAA I Value	Time 2 (Min)	NOAA I Value	Intensity (in/hour)						
	I	ntensity Inter	polation	81.97	60	0.529	120	0.325	0.45						

	EXISTING CONDITIONS HYDROLOGY (100 YEAR)														
SUB-BA	ASIN DATA	INITIAL/O	VERLAND	TIME (Ti)		Overland Flow	Travel Time (Tt)		Tc (Ti+Tt)						
Basin Area	R (C Value)	Length (ft)	Slope	Ti (min)	Length (ft)	Slope	Velocity (fps)	Tt (min)	Tc (min)						
1	1 0.5 100.00 0.811		11.58					11.58							
1					959.90	1.687	0.9	17.77586852	17.78						
1					2701.01	0.696	0.57	78.97675439	78.98						
				SUM TIME	Time 1 (Min)	NOAA I Value	Time 2 (Min)	NOAA I Value	Intensity (in/hour)						
	I	ntensity Inter	polation	108.33	60	1.34	120	0.702	0.83						

	EXISTING CONDITIONS HYDROLOGY (100 YEAR													
SUB-BASIN DATA INITIAL/OVERLAN			VERLAND	TIME (Ti)		Overland Flow	Travel Time (Tt)		Tc (Ti+Tt)					
Basin Area	R (C Value)	Length (ft)	Slope	Ti (min)	Ti (min) Length (ft) Slope Velocity (fps) Tt (min)									
2	0.5	100.00	1.665	9.11					9.11					
2					1112.42	1.635	0.87	21.31073755	21.31					
2					2311.79	1.414	0.82	46.98764024	46.99					
				SUM TIME	Time 1 (Min)	NOAA I Value	Time 2 (Min)	NOAA I Value	Intensity (in/hour)					
	I	ntensity Inter	polation	77.41	60	1.34	120	0.702	1.15					

## Table B - Proposed Conditions - Rational Method Tc=Ti+Tt for Intensity Calculations

(Modified Truckee Meadows Reagional Drainage Manual Table 703)

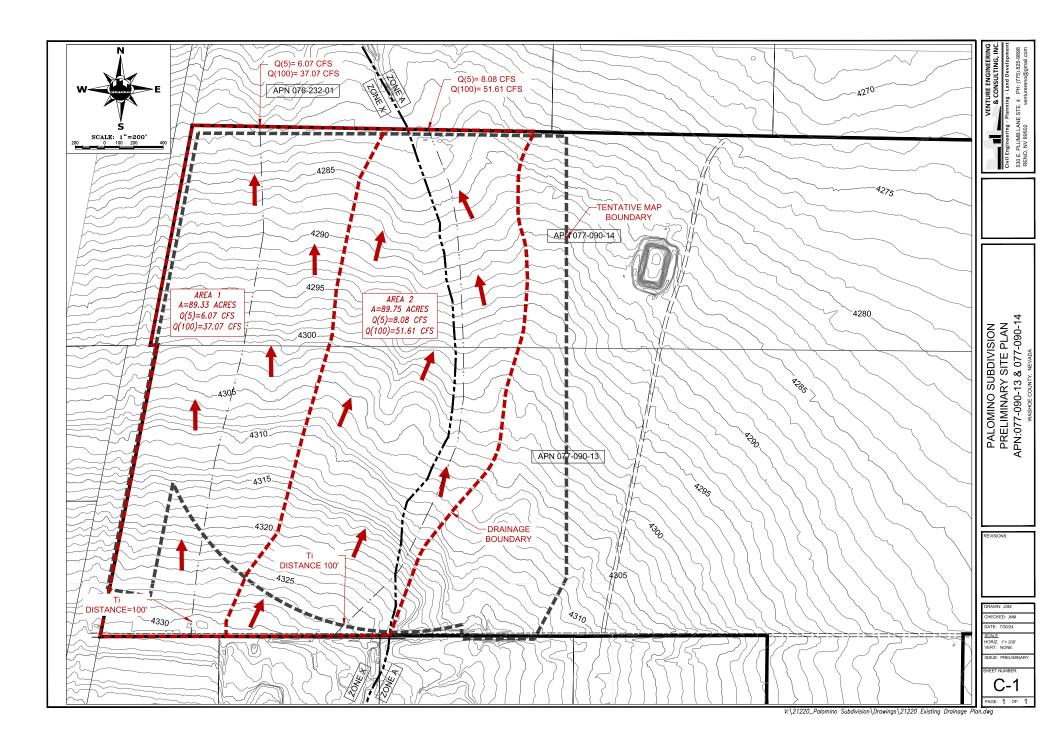
Time Calc
Intensity Calc

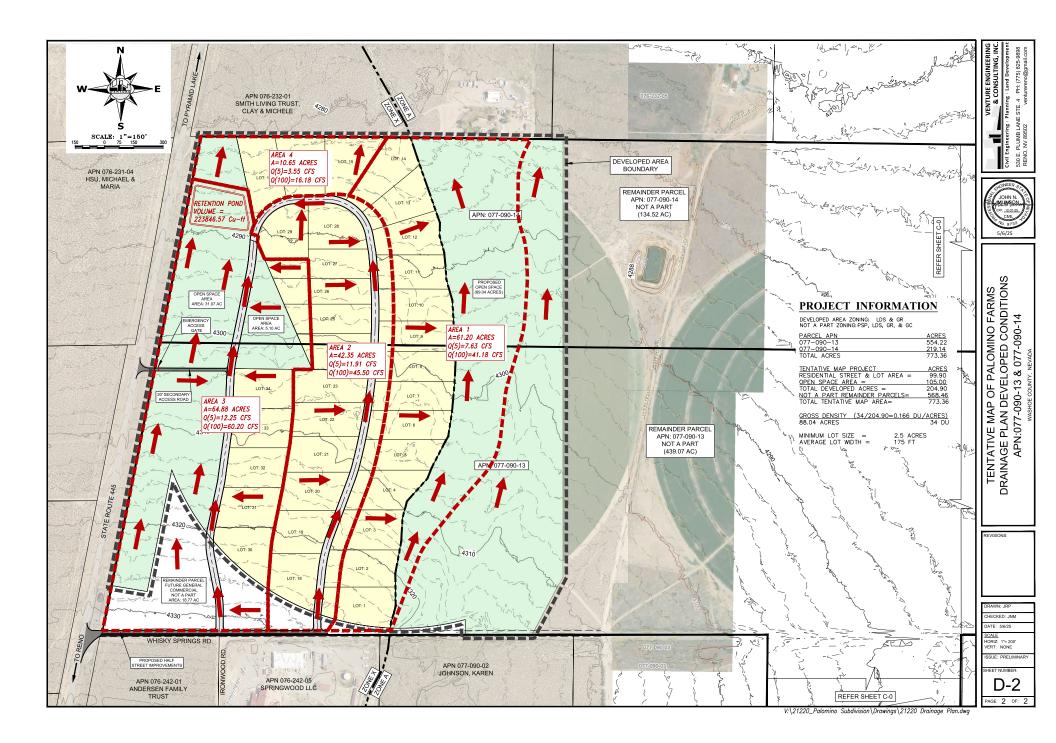
	PROPOSED CONDITIONS HYDROLOGY (5 YEAR)														
SUB-BASIN DATA INITIAL/OVERLAND TIME (Ti) Roadside Ditch Travel Time (Tt) To								Tc (Ti+Tt)	Intensity Interpolation						
Basin Area	R (Composite C)	Length (ft)	Slope	Ti (min)	Length (ft)	Velocity (fps)	Tt (min)	Tc (min)	Time 1 (Min)	NOAA I Value	Time 2 (Min)	NOAA I Value	Intensity (in/hour)		
Area 1	0.28	3491	1.203	82.00				82.00	60	0.529	120	0.326	0.45		
Area 2	0.37	490	1.000	29.09	3904	6.92	9.40	38.49	30	0.854	60	0.529	0.76		
Area 3	0.37	2700	1.481	59.89	2702	6.92	6.51	66.40	60	0.529	120	0.326	0.51		
Area 4	0.32	392	1.786	22.91				22.91	15	1.27	30	0.854	1.05		

	PROPOSED CONDITIONS HYDROLOGY (100 YEAR)												
SUB-BASIN DATA INITIAL/OVERLAND TIME (Ti)					Roadsid	Roadside Ditch Travel Time (Tt)			olation				
Basin Area	R (Composite C)	Length (ft)	Slope	Ti (min)	Length (ft)	Velocity (fps)	Tt (min)	Tc (min)	Time 1 (Min)	NOAA I Value	Time 2 (Min)	NOAA I Value	Intensity (in/hour)
Area 1	0.5	3491	1.203	60.00				60.00	30	2.17	60	1.34	1.34
Area 2	0.51	490	1.000	23.51	3904	6.92	9.40	32.91	30	2.17	60	1.34	2.09
Area 3	0.57	2700	1.481	43.48	2702	6.92	6.51	49.99	30	2.17	60	1.34	1.62
Area 4	0.5	392	1.786	17.63				17.63	15	3.22	30	2.17	3.04

	Existing Condition Hydrology						
	Rational Method Tc=Ti+Tt (Time of Con	centration)					
		ec. i.i. d.i.o.i.y					
	Surface Cover	Area (sf)	<u>C5</u>	Weighted	C100	Weighted	
	Open Space (0-5% vegetated)	7,800,724.80	0.20	1560145	0.5	3900362	
	Total/Composite	7,800,724.80	0.20	1560145	0.50	3900362	
	Acres Total	179.08					
Basin Area	Area (acres)	I(5) in/hr (Tc=Ti+Tt)	<u>C5</u>	Q(5) cfs	<u>C100</u>	I(100) in/hr (Tc=Ti+Tt)	Qp(100) c
1	<u>89.33</u>	0.34	0.20	6.07	0.50	0.83	37.07
2	<u>89.75</u>	0.45	0.20	<u>8.08</u>	0.50	1.15	<u>51.61</u>
Total				<u>14.15</u>			<u>88.68</u>
	Developed Condition Hydrology						
	Rational Method Tc=Ti+Tt (Time of Con	centration)					
	Surface Cover	Area (sf)	<u>C5</u>	Weighted	<u>C100</u>	Weighted	
Area 1	Rural 2.5 Acre lots	1,298,350.73	0.35	454423	0.5	649,175.4	
Area 1	Open space Range	1350907.43	0.2	270181	0.5	675,453.7	
	Commercial Area	16632.51	0.85	14138	0.85	14,137.6	
	Total Area 1	2665890.67	0.28	738742	0.50	1338767	
Area 2	Rural 2.5 Acre lots	1,770,422.11	0.35	619648	0.5	885211	
Area 2	Commercial Area	74,183.17	0.85	63056	0.85	63056	
	Total Area 3	1844605.28	0.37	682703	0.51	948267	
Area 3	Rural 2.5 Acre lots	663,890.12	0.35	232362	0.5	331,945.1	
Area 3	Commercial Area	586996.07	0.85	498947	0.85	498,946.7	
Area 3	Open space Range	<u>1575442.89</u>	0.2	<u>315089</u>	0.5	<u>787,721.4</u>	
	Total Area 3	2826329.08	0.37	1046397	0.57	1618613	
Area 4	Rural 2.5 Acre lots	363,239.40	0.35	127134	0.5	181,619.7	
Area 4	Open space Range	100588.48	0.2	20118	0.5	50,294.2	
	Total Area 4	463827.88	0.32	147251	0.50	231914	
	Area (acres)	I(5) in/hr (Tc=Ti+Tt)	<u>C5</u>	Q(5) cfs	<u>C(100)</u>	I(100) in/hr (Tc=Ti+Tt)	Qp(100) o
Area 1	61.20	0.45	0.28	7.63	0.50	1.34	41.18
Area 2	42.35	0.76	0.37	11.91	0.51	2.09	45.50
Area 3	64.88	0.51	0.37	12.25	0.57	1.62	60.20
Area 4	10.65	<u>1.05</u>	0.32	3.55	<u>0.50</u>	<u>3.04</u>	16.18
	Total Developed Runoff			35.34			163.06
ımmary						Peak Flow	Peak Flo
						35.34	163.06
						Peak Flow	Peak Flov
						Q(5) cfs	Q(100) cf
				Volume	Volume	-14.15	-88.68
crease	Table B Time 5yr (min)	Table B Time 100yr (min)		5-Year, Cu-Ft	100-Year, Cu-Ft	Peak Flow	Peak Flov
	66.4	49.99		84427.36	223107.86	21.19	74.38

		Reten	tion Basin	
	Contour	Contour Area (ft^2)	Contour Interval Height (ft)	Volume (ft^3)
L00 yr)	85.00	97458.65	2.41	223846.57
	82.59	88306.1361	0.00	0.00
			Volume Storage Provided	223846.57
			Storage Required	223107.86





## A = watershed area, acres

The following Table 201 listing runoff coefficients based depending on future use, shall be used:

## TABLE 201 RUNOFF COEFFICIENTS "C"

<u>Land Use Type</u>	Runoff Coefficient "C"
Rural	0.25-0.35
Single Family Residential	0.45-0.60
Multi-Residential	0.60-0.70
Neighborhood Commercial	0.85
Community Commercial	0.85
Tourist Commercial	0.85
Office	0.85
Manufacturing	0.85-0.90
Distribution and Warehousing	0.85-0.90
Public Facility	0.50-0.85
Pavement and Concrete Surfaces	0.90-0.95
Park	0.25
Open Space (0-5% grade - vegetated)	0.20-0.30
Open Space (0-5% grade - no vegetation	)0.30-0.40
Open Space(5-15% grade - vegetated or unvegetated	
Open Space(Over 15% grade - sparsely vegetated, ro	0.40-0.60 ock or clay soils)

City of Reno Public Works Design Manual Weighted values of the runoff coefficient "C" may be required where land use is most accurately described as a mixture of the land uses listed above or where it is a mixture of impervious and pervious areas and not well represented by a single entry in the preceding list.

Sub-areas which include an LID feature will typically require special consideration and weighting of the runoff coefficient "C". See Chapter X for specific guidance on post construction storm water quality design considerations.

Included below for reference is Table 202 from both the TMRDM and the Truckee Meadows Structural Controls Manual.

# TABLE 202 ADDITIONAL RUNOFF COEFFICIENTS "C" FOR REFERENCE

Runoff coefficients for the Rational Method from the Washoe County Hydrologic Criteria and Drainage Design Manual (a.k.a., the TMRDM) and the City of Sparks (1998 and 1996, respectively), and as per the Truckee Meadows Structural Controls Design Manual.

#### **Runoff Coefficients**

Land Use or Surface Characteristics	Aver. % Impervious Area	5-Year (C <sub>s</sub> )	100-Year (C <sub>100</sub> )
Business/Commercial:			
Downtown Areas	85	.82	.85
Neighborhood Areas	70	.65	.80
Residential:			
(Average Lot Size)			
1/8 Acre or Less (Multi-U	Init) 65	.60	.78
<sup>1</sup> / <sub>4</sub> Acre	38	.50	.65
⅓ Acre	30	.45	.60
½ Acre	25	.40	.55
1 Acre	20	.35	.50
Industrial:	72	.68	.82
Open Space:			
(Lawns, Parks, Golf Courses)	5	.05	.30
Undeveloped Areas:			
Range	0	.20	.50
Forest	0	.05	.30
Streets/Roads:			
Paved	100	.88	.93
Gravel	20	.25	.50
Drives/Walks:	95	.87	.90
Roofs:	90	.85	.87
Notes:			

Composite runoff coefficients shown for Residential, Industrial, and Business/Commercial Areas assume irrigated
grass landscaping for all previous areas. For development with landscaping other than irrigated grass, the
designer must develop project specific composite runoff coefficients from the surface characteristics presented in
this table.

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Data Server GIS Grids Maps Time Series

Temporals Documents **Probable Maximum** 

#### Precipitation Documents

Miscellaneous Publications Storm Analysis

Record Precipitation

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#### NOAA ATLAS 14 POINT PRECIPITATION FREQUENCY ESTIMATES: NV

#### Data type: Precipitation intensity ✓ Units: English ✓ Time series type: Partial duration Select location 1) Manually: a) By location (decimal degrees, use "-" for S and W): Latitude: Submit Longitude: b) By station (list of NV stations): Select station

Q

#### 2) Use map:

c) By address Search

PF tabular

PF graphical

**Data description** 



#### POINT PRECIPITATION FREQUENCY (PF) ESTIMATES

WITH 90% CONFIDENCE INTERVALS AND SUPPLEMENTARY INFORMATION NOAA Atlas 14, Volume 1, Version 5

Supplementary information

	PF tabular	PF gr	aphical _	Supplement	tary information			Print page		
	PD	S-based pre	ecipitation fr	equency es	timates with	90% confid	lence interv	als (in inche	s/hour) <sup>1</sup>	
Donation	Average recurrence interval (years)									
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>1.21</b> (0.996-1.39)	<b>1.50</b> (1.24-1.76)	<b>2.02</b> (1.68-2.39)	<b>2.52</b> (2.09-3.01)	<b>3.36</b> (2.75-4.09)	<b>4.16</b> (3.34-5.16)	<b>5.11</b> (4.01-6.46)	<b>6.30</b> (4.76-8.12)	<b>8.23</b> (5.94-11.0)	<b>10.0</b> (6.96-13.
10-min	<b>0.918</b> (0.750-1.06)	<b>1.15</b> (0.936-1.34)	<b>1.54</b> (1.27-1.82)	<b>1.91</b> (1.59-2.29)	<b>2.56</b> (2.09-3.12)	<b>3.17</b> (2.54-3.92)	3.89 (3.05-4.92)	<b>4.79</b> (3.62-6.19)	<b>6.26</b> (4.52-8.36)	<b>7.63</b> (5.30-10.
15-min	<b>0.760</b> (0.620-0.876)	<b>0.948</b> (0.772-1.11)	<b>1.27</b> (1.05-1.50)	<b>1.58</b> (1.32-1.89)	<b>2.12</b> (1.73-2.58)	<b>2.62</b> (2.10-3.24)	<b>3.22</b> (2.52-4.06)	<b>3.96</b> (3.00-5.11)	<b>5.18</b> (3.74-6.91)	<b>6.30</b> (4.38-8.6
30-min	<b>0.512</b> (0.418-0.592)	<b>0.638</b> (0.520-0.746)	<b>0.854</b> (0.710-1.01)	<b>1.07</b> (0.886-1.28)	<b>1.42</b> (1.16-1.74)	<b>1.76</b> (1.41-2.18)	<b>2.17</b> (1.70-2.74)	<b>2.67</b> (2.02-3.44)	<b>3.49</b> (2.52-4.66)	<b>4.25</b> (2.95-5.8
60-min	<b>0.316</b> (0.259-0.366)	<b>0.394</b> (0.322-0.462)	<b>0.529</b> (0.439-0.628)	<b>0.660</b> (0.548-0.789)	<b>0.881</b> (0.720-1.07)	1.09 (0.874-1.35)	<b>1.34</b> (1.05-1.69)	<b>1.65</b> (1.25-2.13)	<b>2.16</b> (1.56-2.88)	<b>2.63</b> (1.82-3.5
2-hr	<b>0.203</b> (0.177-0.237)	<b>0.253</b> (0.221-0.295)	<b>0.326</b> (0.283-0.381)	<b>0.392</b> (0.336-0.457)	<b>0.495</b> (0.415-0.581)	<b>0.590</b> (0.483-0.697)	<b>0.702</b> (0.560-0.855)	<b>0.866</b> (0.661-1.08)	<b>1.14</b> (0.832-1.46)	<b>1.41</b> (0.985-1.8
3-hr	<b>0.160</b> (0.142-0.184)	<b>0.199</b> (0.177-0.230)	<b>0.251</b> (0.222-0.289)	<b>0.295</b> (0.259-0.340)	<b>0.358</b> (0.310-0.414)	<b>0.415</b> (0.352-0.484)	<b>0.484</b> (0.403-0.573)	<b>0.583</b> (0.475-0.723)	<b>0.770</b> (0.595-0.978)	<b>0.945</b> (0.705-1.2

6-hr	<b>0.111</b> (0.099-0.126)	<b>0.138</b> (0.123-0.158)	<b>0.173</b> (0.153-0.197)	<b>0.199</b> (0.176-0.227)	<b>0.235</b> (0.205-0.269)	<b>0.261</b> (0.225-0.301)	<b>0.289</b> (0.246-0.336)	<b>0.326</b> (0.273-0.384)	<b>0.402</b> (0.330-0.495)	<b>0.477</b> (0.384-0.617)
12-hr	<b>0.072</b> (0.064-0.081)	<b>0.090</b> (0.081-0.102)	<b>0.115</b> (0.102-0.129)	<b>0.133</b> (0.118-0.150)	<b>0.158</b> (0.139-0.180)	<b>0.178</b> (0.154-0.203)	<b>0.198</b> (0.170-0.228)	<b>0.218</b> (0.184-0.254)	<b>0.245</b> (0.202-0.291)	<b>0.271</b> (0.219-0.326)
24-hr	<b>0.044</b> (0.039-0.050)	<b>0.056</b> (0.050-0.063)	<b>0.073</b> (0.065-0.082)	<b>0.087</b> (0.077-0.098)	<b>0.106</b> (0.093-0.120)	<b>0.121</b> (0.105-0.138)	<b>0.137</b> (0.118-0.158)	<b>0.154</b> (0.130-0.179)	<b>0.178</b> (0.147-0.209)	<b>0.197</b> (0.160-0.234)
2-day	<b>0.026</b> (0.023-0.029)	<b>0.033</b> (0.029-0.038)	<b>0.044</b> (0.039-0.050)	<b>0.052</b> (0.046-0.060)	<b>0.065</b> (0.056-0.074)	<b>0.074</b> (0.064-0.086)	<b>0.085</b> (0.072-0.099)	<b>0.096</b> (0.080-0.113)	<b>0.112</b> (0.091-0.133)	<b>0.124</b> (0.099-0.151)
3-day	<b>0.019</b> (0.017-0.021)	<b>0.024</b> (0.021-0.028)	<b>0.032</b> (0.028-0.037)	<b>0.039</b> (0.034-0.044)	<b>0.048</b> (0.042-0.055)	<b>0.056</b> (0.048-0.065)	<b>0.064</b> (0.054-0.075)	<b>0.073</b> (0.060-0.086)	<b>0.085</b> (0.069-0.102)	<b>0.095</b> (0.075-0.116)
4-day	<b>0.015</b> (0.013-0.017)	<b>0.020</b> (0.017-0.023)	<b>0.027</b> (0.023-0.030)	<b>0.032</b> (0.028-0.037)	<b>0.040</b> (0.034-0.046)	<b>0.047</b> (0.039-0.054)	<b>0.054</b> (0.045-0.063)	<b>0.061</b> (0.050-0.072)	<b>0.072</b> (0.058-0.086)	<b>0.081</b> (0.064-0.098)
7-day	<b>0.010</b> (0.009-0.012)	<b>0.013</b> (0.011-0.015)	<b>0.018</b> (0.015-0.021)	<b>0.022</b> (0.019-0.025)	<b>0.027</b> (0.023-0.032)	<b>0.032</b> (0.027-0.037)	<b>0.037</b> (0.030-0.043)	<b>0.042</b> (0.034-0.050)	<b>0.049</b> (0.039-0.060)	<b>0.055</b> (0.043-0.068)
10-day	<b>0.008</b> (0.007-0.009)	<b>0.010</b> (0.009-0.012)	<b>0.014</b> (0.012-0.016)	<b>0.017</b> (0.015-0.020)	<b>0.021</b> (0.018-0.025)	<b>0.025</b> (0.021-0.029)	<b>0.028</b> (0.023-0.033)	<b>0.032</b> (0.026-0.038)	<b>0.037</b> (0.030-0.045)	<b>0.042</b> (0.033-0.051)
20-day	<b>0.005</b> (0.004-0.006)	<b>0.006</b> (0.005-0.007)	<b>0.009</b> (0.007-0.010)	<b>0.010</b> (0.009-0.012)	<b>0.013</b> (0.011-0.015)	<b>0.015</b> (0.012-0.017)	<b>0.016</b> (0.014-0.019)	<b>0.018</b> (0.015-0.022)	<b>0.021</b> (0.017-0.026)	<b>0.024</b> (0.019-0.029)
30-day	<b>0.004</b> (0.003-0.004)	<b>0.005</b> (0.004-0.006)	<b>0.007</b> (0.006-0.008)	<b>0.008</b> (0.007-0.009)	<b>0.010</b> (0.008-0.011)	<b>0.011</b> (0.009-0.013)	<b>0.012</b> (0.010-0.015)	<b>0.014</b> (0.011-0.016)	<b>0.016</b> (0.013-0.019)	<b>0.018</b> (0.014-0.021)
45-day	<b>0.003</b> (0.002-0.003)	<b>0.004</b> (0.003-0.004)	<b>0.005</b> (0.004-0.006)	<b>0.006</b> (0.005-0.007)	<b>0.008</b> (0.006-0.009)	<b>0.009</b> (0.007-0.010)	<b>0.010</b> (0.008-0.011)	<b>0.011</b> (0.009-0.012)	<b>0.012</b> (0.010-0.014)	<b>0.013</b> (0.011-0.016)
60-day	<b>0.002</b> (0.002-0.003)	0.003 (0.003-0.004)	<b>0.004</b> (0.004-0.005)	<b>0.005</b> (0.004-0.006)	<b>0.006</b> (0.005-0.007)	<b>0.007</b> (0.006-0.008)	<b>0.008</b> (0.007-0.009)	<b>0.009</b> (0.007-0.010)	<b>0.010</b> (0.008-0.011)	<b>0.010</b> (0.008-0.012)

<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

Estimates from the table in CSV format: Precipitation frequency estimates ▼ Submit

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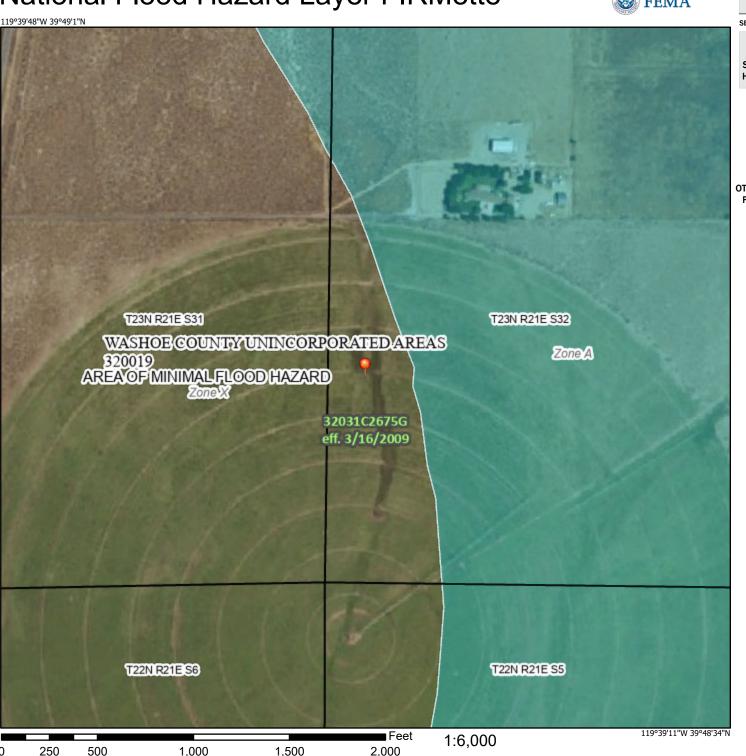
US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service Office of Water Prediction (OWP) 1325 East West Highway Silver Spring, MD 20910 Page Author: HDSC webmaster Page last modified: April 21, 2017

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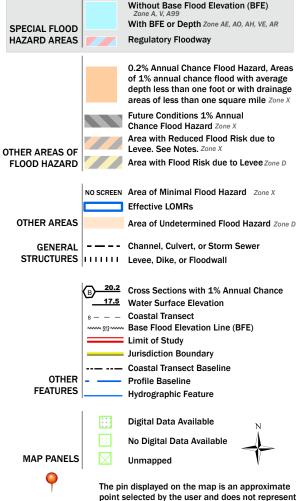
## National Flood Hazard Layer FIRMette





#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 9/3/2024 at 11:33 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

Venture Engineering & Consulting Inc. 530 E. Plumb Lane Reno, NV 89502

Phone: (775) 825-9898

May 8, 2025

Washoe County Community Development City of Reno 1001 E 9th St Reno, NV 89512

Re: Palomino Farms Tentative Map Traffic Estimate.

As part of the tentative map application for the proposed 34-lot subdivision, estimated trip generation rates have been reviewed in accordance with Washoe County requirements. Based on standard assumptions from the 11<sup>th</sup> edition ITE traffic formulas for an average rate of 0.75 AM peak hour trips and 0.99 PM peak hour trips per single-family lot, the project is expected to generate approximately 26 AM and 34 PM peak hour trips on a typical weekday. These projected volumes are well below the threshold of 80 peak hour trips that would require a traffic impact report under County standards—representing only about 3/7 of the minimum requirement. While some residents at the recent neighborhood meeting raised concerns and requested a traffic study, the anticipated traffic generation does not meet the criteria necessitating one for this application.

Any future traffic analysis related to improvements at the intersection of Whiskey Springs Road and Pyramid Highway (State Route 431) will fall under the purview of the Nevada Department of Transportation (NDOT).

Sincerely,

VENTURE ENGINEERING AND CONSULTING. INC.

John N. Munson, P.E.

President/Principal

# Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

**AM Peak Hour of Generator** 

Setting/Location: General Urban/Suburban

Number of Studies: 169
Avg. Num. of Dwelling Units: 34

Directional Distribution: 26% entering, 74% exiting

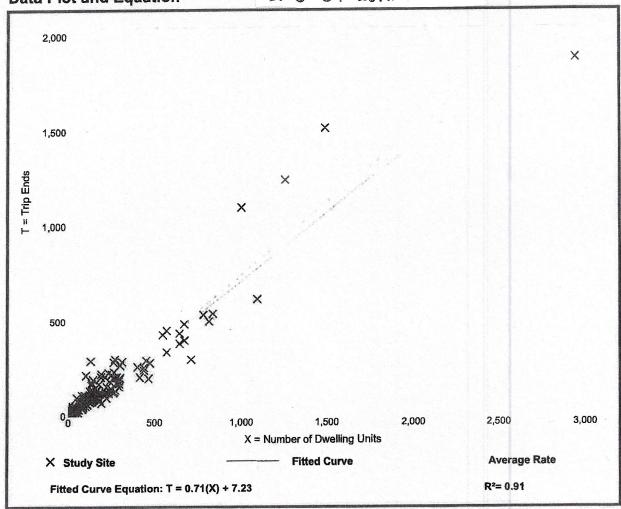
## Vehicle Trip Generation per Dwelling Unit

Average Rate 0.75 Range of Rates 0.34 - 2.27 Standard Deviation

0.25

## **Data Plot and Equation**

0.75 × 34 = 26 AM PHT



Trip Gen Manual, 11th Edition

Institute of Transportation Engineers

# Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

PM Peak Hour of Generator

Setting/Location: General Urban/Suburban

178 Number of Studies:

34 Avg. Num. of Dwelling Units:

Directional Distribution: 64% entering, 36% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate

Range of Rates

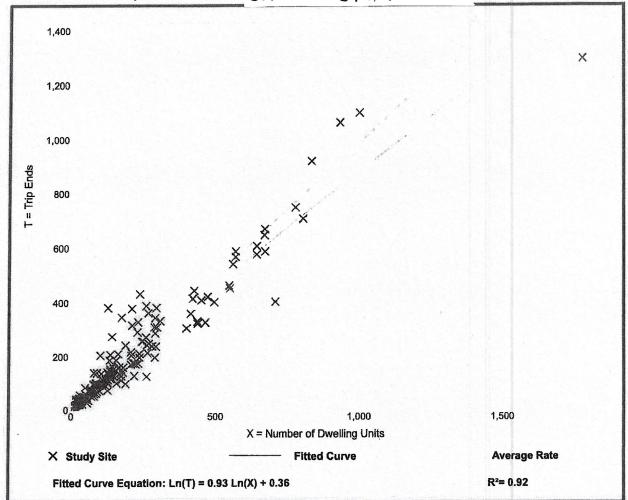
0.49 - 2.98

Standard Deviation

0.28

### **Data Plot and Equation**

0.99 × 34 = 34 PM PHT



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